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	+ advertising fee	
Development Applications > 80m ²	\$285 + \$1.50/m ²	
	+ advertising fee	
Level 2 Activity	\$2,075	
	+ advertising fee by quote	
SUBDIVISION	\$370 + \$60/lot	
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App. No.
PID
Log In No.
Receipt No.
Receipt Date:
Fee \$

PLANNING PERMIT APPLICATION APPLICATION FOR PLANNING APPROVAL UNDER SECTION 51, LAND USE PLANNING & APPROVALS ACT 1993

Full Name of Appl Postal Address of Would you like thi	icant(s)PO Box 63 Rive	rside TAS 7250
Would you like thi	PO Box 63 Rive Applicants(s)	rside TAS 7250
	is address recorded for all Cour	
		ncil correspondence Yes No
		0417 921 661 Mobile
In accordance with the owner of the la	and in respect of which the permit is	and Approvals Act 1993 if the applicant for the permit is not srequired, the applicant must include in the application for the owner of the intention to make the application.
relevant Crown Mir the Minister/Gener		
Full Name	C J and R S Kelly	G A Medwin and D R Medwin
Address	PO Box 780 Devonport TAS 73	PO Box 3025 Burnie TAS 7320
Telephone – F	lome	
Applicant's Notifica	ation to Owner	
Full Name of Applic	ant(s) .td	
of		
Declare that I/we	have notified the owner(s) of the pro	operty(ies) of the intention to make this application.
must not obtain o		2) of the Land Use Planning and Approvals Act 1993 a personully making, or causing to be made, any false representation

Э.	Proposed Development (rully describe intended use or land or premises)
	Demolition of existing dwelling, replacement dwelling and construction of retaining walls.
6.	Supporting Information if necessary to explain special features of the proposal. (Attach separate sheet if required)
	Please refer to the planning submission.
	To include – (a) Two Copies (4 electronic copy if available) of any plan(a) and (an energification(a) for the ground and
	(a) Two Copies (+ electronic copy if available) of any plan(s) and/or specification(s) for the proposed development, showing where applicable:
	 i. Sufficient information to demonstrate compliance with all applicable standards, purpose statements in applicable zones and codes, any relevant local area objectives or desired future character statements;
	☐ ii. a full description of the proposed use or development;
	 iii. a full description of the manner in which the use or development will operate; iv. a site analysis and site plan at an acceptable scale;
	\square v. a detailed layout plan of the proposed buildings with dimensions at a scale of 1:100 or 1:200;
	vi. a plan of the proposed landscaping;vii. car parking facilities and capacity;
	☐ viii. area of clearing of trees and bushland;
	\square ix. size, position, colour, illumination, fixing or support and other design details of advertising sign(s).
	(b) A FULL COPY OF YOUR TITLE SHALL ALSO ACCOMPANY THE APPLICATION.
	Title Certificate Title Plan Schedule of Easements
	(c) RELEVANT ENGINEERING APPROVALS
	Access Stormwater
7.	Present use of site and/or buildings – full description
	Residential
8.	Car Parking Floor Area Site Area
	Existing on site Existing m^2
	Total no. proposed Proposed m²
	Total 80 m²

N	Monday to Friday:	From	a.m. to	p.m.
	Saturday:	From	a.m. to	p.m.
	Sunday:	From	a.m. to	p.m.
10. N	Number of Employees?			
Ε	Existing			
P	roposed			
11. V	⁷ ehicles visiting or deliv	ering to or from the site?		
Т		No.	Trips per day	
	What type of machinery Type	is to be installed or used? No.		
T' 		No.		
ARATION TO THE TRANSPORT THE T	ON BY APPLICANT (months) of the information given that the Council may make the communication and assessment of that app	No. is a true and accurate representation provided with the development applicates such copies of the information and fithe Permit Application. I have obtain reproduction of the plans accompalication. I indemnify the Waratah-Wy	ation may be made availal d materials as in its opinion ned the relevant permission nying the development a nyard Council for any cla	ole to the pu on are neces on of the co application f
ARATION TO THE STATE OF THE STA	ON BY APPLICANT (months) The information given by the communication and materials proposed that the council may make the communication and assessment of that appressed of breach of copy acknowledge that Second the General Manager permit or other approved.	No. is a true and accurate representation provided with the development applicable such copies of the information and fithe Permit Application. I have obtain reproduction of the plans accompalication. I indemnify the Waratah-Wyyright in respect of any of the information and the content and without notice in relation to the land without notice in relation.	ation may be made availally discretized as in its opinion ned the relevant permission of the development at any arranged Council for any clasion or material provided. Act 1993 provides the part of the any application by the	ole to the pure name necession of the complete of application of the complete of the pure

OFFICE USE ONLY

14.	Application Taken on	Ву
15.	Application given o.k. to process	Ву
16	Use Class	
17.	Zoning of Property	
18.	Proposal	
19.	Permit Type Advertisement Date	
19.	Discretion	
20.	Notice on Property by at	am/pm
(On(see declaration attached)
21.	Immediate Adjoining Property Owner(s) Notified on	
22.	Gas Pipeline Che	ecked By
23.	Heritage ListedChe	ecked By
24.	Assessment Committee for Dam Construction	ecked By
25	Prime Agricultural Land	ecked By
	Land Hazard Low	ecked By
27.	Landslip A Landslip B Landslip Susceptibility Che	ecked By
28.	Clock Started	
29.	42 Days run out on:	Checked By
30.	Extension of Time Until	
31.	Application - Approved/Refused	
32.	Decision Date	
33.	Applicant(s) Notified	
34.	Representor(s) Notified	



7 June 2018

Enquiries: Tow Phone: (03)

Townplanner (03) 6443 8305

Our Ref:

7087735 & DA 53/2018

6ty Pty Ltd PO Box 63 RIVERSIDE TAS 7250

Dear George,

ADDITIONAL INFORMATION REQUIRED
DEVELOPMENT APPLICATION – Demolition of existing dwelling, replacement dwelling and retaining walls
15 Hepples Road and 13 Hepples Road BOAT HARBOUR BEACH

I advise that under Section 54 of the Land Use Planning and Approvals Act 1993 Council seeks further information in relation to application DA 53 for a Demolition of existing dwelling, replacement dwelling and retaining walls at 15 Hepples Road and 13 Hepples Road BOAT HARBOUR BEACH. In order to progress the assessment of your application, please provide the following:-

- Proposal drawings of new replacement dwelling at an appropriate scale at an A3 Page size. Current drawings provided are dimensioned and in proportion but not at a measureable scale.
- Proposal drawings showing a new retaining wall are not clearly marked with an appropriate scale. Please provide details with an elevation view and section of all retaining walls at an appropriate scale. No details have been provided to date for the retaining wall crossing the boundary of 13 and 15 Hepples Road.
- Demonstration of compliance with clause 12.4.1 (P2) Suitability of a site lot for use or development of the Waratah-Wynyard Interim Planning Scheme 2013. Furthermore, how is the site to be accessed for the development works?
- Demonstration of compliance with 12.4.1 A3/P3 Suitability of a site or lot for use or development of the Waratah-Wynyard Interim Planning Scheme 2013. Please confirm arrangements for water.
- Demonstration of compliance with 12.4.3 A1/P1 and A2/P2 Location and configuration of development of the *Waratah-Wynyard Interim I Janning Scheme 2013*, in relation to the retaining walls. The retaining walls are treated as building works under the Act.

- Demonstration of compliance with the Hazard Management Code of the Waratah-Wynyard Interim Planning Scheme 2013, in relation to the works proposed and occurred to date. The subject Geotechnical report must indicate the proposed development can achieve and maintain a tolerable level of risk for the duration of the development. The current report states that no development drawings had been considered as they had not yet been provided. This report will need to take into consideration the demolition works, retaining walls, earthwork, and the proposed new dwelling as detailed in the drawings provided.
- Demonstration of compliance with clause E4.6.1 A1/P1 Change in existing ground level or natural ground level of the *Waratah-Wynyard Interim Planning Scheme 2013*. Supporting documentation in the current Geotechnical report suggests cuts ranging from approximately 1.5m to 1 story have occurred. Sections through the site (lots) to demonstrate cut and fill and proposed levels with section marks identifying the cuts on the site plan would assist a response to this clause. Please provide details in relation to any Part V agreement arrangements if unable to achieve compliance with A1 (g).
- Demonstration of compliance with clause E10.6.2 P1 Development in a shoreline area of the *Waratah-Wynyard Interim Planning Scheme 2013*, as the proposed dwelling replacement is located within 30m of the mean high tide water mark.

Your application has been placed on hold until all relevant documentation has been received to the satisfaction of the Planning Authority.

If you have any queries or require further information, please do not hesitate in contacting myself, on (03) 6443 8305.

Yours faithfully

Mathew Jamieson

ACTING MANAGER DEVELOPMENT & REGULATORY SERVICES



Planning Submission

Residential Dwelling
13 and 15 Hepples Road, Boat Harbour

Prepared for:

Waratah-Wynyard Council



Measured form and function 6ty

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Issue	02	
Date	13 February 2019	
Project Name	Hepples Road Dwelling	
Project Number	17.077	
Author	George Walker	
Document	Response to Council Request for Further Information	



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Appendix A

Certificate of Title

Appendix B

Development Plans

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Landslide Risk Assessment



1.0 Introduction

Planning approval is sought to demolish an existing dwelling and construct a new dwelling and retaining walls on land located at 13 and 15 Hepples Road, Boat Harbour (the site - refer to Figure 1). This planning submission provides relevant details of the application and an assessment against the applicable provisions of the Waratah-Wynyard Interim Planning Scheme 2013 (the Scheme).

Site

Figure 1 - aerial image identifying the site.

Source: base image and data from the LIST (www.thelist.tas.gov.au) © State of Tasmania.

1.1 Planning Overview

Element	Overview
Location	13 and 15 Hepples Road, Boat Harbour
Title Information	143923/32 and 143923/31
Land Area	568.1m ²
Planning Instrument	Waratah-Wynyard Interim Planning Scheme 2013 (the Scheme)
Proposed Use	Residential
Proposed Development	Demolition of an existing dwelling and construction of a new dwelling and retaining walls

Zone(s) 12.0 - Low Density Residential	
, ,	E4.0 - Change in Ground Level Code E6.0 - Hazard Management Code E9.0 - Traffic Generating Use and Parking Code E10.0 - Water and Waterways Code
Status of Application	Discretionary

1.2 Background

Aspects of the proposed development have been carried out without obtaining relevant planning and building approvals which include partial demolition of the existing dwelling, partial construction of the new dwelling and construction of the two new retaining walls (refer to Figures 2 and 3). Retrospective planning approval is therefore sought for development that has occurred without obtaining the necessary planning approvals.

Figure 2 - photograph showing the extent of partial demolition of the existing dwelling and construction of the new dwelling that has already occurred.





Figure 3 - photograph showing the as constructed 'verti-block' retaining wall.

1.3 Proposed Use and Development

The application seeks approval to demolish an existing residential dwelling and construct a new dwelling and two retaining walls at the site. Details of the proposed use and development are summarised below.

Demolition of existing dwelling

The existing dwelling is split level with an overall height of approximately 5.6m above existing ground level. It has a skillion roof which slopes downwards toward the southwest. The ground floor level is approximately $14m^2$ in area and comprises two bedrooms. The first floor level is approximately $111m^2$ in area and comprises an open plan kitchen, dining and living area, two bedrooms, bathroom and laundry. A deck extends around the north-western and north-eastern sides of the dwelling. The deck abuts the north-western boundary. A stair case is located on the south-eastern side of the deck which provides access between the two levels. It is proposed to demolish the entire dwelling.

Construction of new dwelling

The proposed dwelling will be two storey and will be constructed over a similar footprint as the existing dwelling. The ground floor level will have an area of approximately 88m² and will comprise a family room, two bedrooms, bathroom and an outdoor patio which will be located below the first floor level. An internal staircase will be located at the south-western end of the building which will provide access between the two levels.

The first floor level will have an area of approximately 117m² and will comprise an open plan living dining and kitchen area and master bedroom which will include an ensuite. A deck will extend around the north-western and north-eastern elevations with access to be provided via a glass sliding door from the open plan living area. It will be constructed to the north-western boundary.

The proposed dwelling will have a gabled roof which will result in an overall building height of 7.1m above existing ground level. The external walls of the ground floor level will be formed of poured concrete panels with the external walls of the first floor level to be clad with fibre cement sheeting or horizontal weatherboards. The deck will be timber framed and will incorporate a glazed balustrade. Privacy screens will be located along the north-western and south-eastern ends of the deck. A stair case is located on the south-eastern side of the deck to provide external access between the ground floor and first floor levels.

Retaining walls

The existing pedestrian access which runs below Hepples Road adjacent to the established concrete crib retaining wall has been modified. The retaining wall incorporates bored piers and has been cast in no fines concrete with a beam placed on top of the structure which forms the footpath. The concrete retaining wall continues parallel to the north-western boundary for the length of the dwelling. The wall be setback 1m from the north-western boundary.

A 'verti-block' retaining wall extends diagonally from the south-eastern corner of the retaining wall that contains the pedestrian walkway. It is constructed of pre-cast concrete mass blocks. Approximately 4m of the retaining wall extends into the adjacent lot to the south-east which is addressed as 13 Hepples Road.



2.0 Location

2.1 Subject Site

The site is located on the eastern (lower) side of Hepples Road and is approximately 568.1m² in area. It comprises two (2) separate lots. 13 Hepples Road (CT 143923/32) is 308.2m² in area and has a 13.5m wide frontage to Hepples Road. It contains an existing dwelling. No works are proposed to this dwelling. Approximately 4m of the 'verti-block' retaining wall will be located on this lot.

15 Hepples Road (CT 143923/31) is 268.5m² in area and has a 18m wide frontage to Hepples Road. A pipeline easement 1m in width runs parallel to the north-western boundary of the lot. The majority of works proposed will occur on this lot.

Land within the site drops away acutely from Hepples Road. The surface level of the existing dwellings is therefore approximately 7.5m below the pavement of Hepples Road. An existing concrete crib retaining wall is located along the frontage of the site which supports Hepples Road above.

Due to the acute level change between the road and the lot, vehicular access and parking is unable to be provided. Existing pedestrian access is provided in the south-eastern corner of the site via a concrete walkway which abuts the crib retaining wall.

The site adjoins similar sized lots to the north-west and south-east which both contain dwellings. The Boat Harbour Beach coastal reserve adjoins the north-eastern-boundary of the site.

2.2 Description of the Surrounding Area

The site is located within the south-eastern section of the Boat Harbour Beach coastal settlement which is zoned Low Density Residential (refer to Figure 4). The settlement is located within a band of land that lies between the coastline to the north and north-east and escarpment to the west. The site is located at the south-eastern end of the settlement area.

The settlement is primarily characterised by residential use and development. It also includes a surf lifesaving club in the northern half adjacent to the main beach. A public car park and toilet block are located to the north of the surf lifesaving club.

Site

Figure 4 - aerial image showing the extent of the Boat Harbour Beach settlement area which is zoned Low Density Residential and the location of the site.

Source: base image and data from the LIST (www.thelist.tas.gov.au) © State of Tasmania.

2.3 Natural Values and Hazards

The site has been substantially modified to accommodate the established residential dwelling and is therefore cleared of significant native vegetation. TASVEG 3.0 mapping identifies the development areas within the settlement area as 'urban'. The site is not within an area that is subject to coastal inundation, erosion or recession on the Scheme overlay maps.

The site is located within a proclaimed landslip area. Accordingly a Landslide Risk Assessment has been prepared by Tasman Geotechnics for the purposes of addressing the Hazard Management Code of the Scheme. The risk assessment has determined that there will be no increase in the landslip risk profile as a result of the proposed development.

2.4 Site Servicing

The new dwelling will utilise existing water, stormwater and sewerage connections.

2.5 Site Access

The site has frontage to Hepples Road which is a local road under the authority of Council. However, due to the acute change in surface level between the road and the body of the lot, vehicular access is not available. Existing pedestrian access is



provided in the south-eastern corner of the site. Large and more cumbersome construction materials will be transferred from Hepples Road to the site by crane with smaller construction materials to be carried down the pedestrian access.



3.0 Planning Assessment

The following assessment addresses the applicable zone and code provisions and identifies whether the relevant acceptable solutions are satisfied. The relevant performance criteria are addressed in Section 4.

For the purposes of the assessment against the zone provisions, the site represents 15 Hepples Road. The length of retaining wall that extends into 13 Hepples Road has not been considered within the following assessment. Further, the assessment is based on the state of the site prior to the illegal works being undertaken.

3.1 Low Density Residential Zone

Residential use for a single dwelling is identified as 'permitted' in the Low Density Residential zone. The proposed development meets the acceptable solutions for most of the standards in the zone that are relevant, as identified in the following table.

12.4	12.4 Development Standards				
Rec	quirement/s	Assessment	Compliance		
12.4.1 Suitability of a site or lot for use		or development			
A1	A site or each lot on a plan of subdivision must –	268.5m ² and is unable to	performance		
	(a) have an area of -	contain a building area ¹ of not less than 10m by 15m in	criteria.		
	(i) not less than 500m ² excluding any access strip;	a location that is clear of applicable side and rear setbacks.			
	(ii) if in a locality shown in the Table to this clause, not less than the site area shown for that locality; and				
	(b) contain a building area of not less than 10.0m x 15.0m -				
	(i) clear of any applicable setback from a frontage, side or rear boundary;				
	(ii) clear of any applicable setback from a zone boundary;				

¹ In accordance with clause 4.1 of the Scheme, building area means the area shown on a plan or plan of subdivision to indicate where all buildings will be located.

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12.4	4 Development Standards		
Red	quirement/s	Assessment	Compliance
	(iii) clear of any registered easement;		
	(iv) clear of any registered right of way benefitting other land;		
	(v) clear of any restriction imposed by a utility;		
	(vi) not including an access strip;		
	(vii) accessible from a frontage or access strip; and		
	(viii) if a new residential lot, with a long axis within the range 30o east of north and 20o west of north.		
A2	A site or each lot on a subdivision plan must have a separate access from a road –	The site has access across an existing frontage to Hepples Road which is 18m in width. Advice from Council, being the relevant road authority for Hepples	Complies with acceptable solution.
	(a) across a frontage over which no other land has a right of access; and		
	(b) if an internal lot, by an access strip connecting to a frontage over land not required as the means of access to any other land; or	Road, is sought in conjunction with the development application.	
	(c) by a right of way connecting to a road -		
	(i) over land not required as the means of access to any other land; and		
	(ii) not required to give the lot of which it is a part the minimum properties of a lot in accordance with the acceptable solution in		



12.4	12.4 Development Standards				
Red	quirement/s	Assessment	Compliance		
	any applicable standard; and				
	(d) with a width of frontage and any access strip or right of way of not less than -				
	(i) 3.6m for single dwelling development; or				
	(ii) 6.0m for multiple dwelling development or development for a non-residential use; and				
	(e) the relevant road authority in accordance with the Local Government (Highways) Act 1982 or the Roads and Jetties Act 1935 must have advised it is satisfied adequate arrangements can be made to provide vehicular access between the carriageway of a road and the frontage, access strip or right of way to the site or each lot on a proposed subdivision plan.				
A3	A site or each lot on a plan of subdivision must be capable of connecting to a water supply – (a) provided in accordance with the Water and Sewerage Industry Act 2008; or	The site has an existing connection to a water supply which has been provided in accordance with the Water and Sewerage Industry Act 2008.	Complies with acceptable solution.		
	(b) from a rechargeable drinking water system [R4] with a storage capacity of not less than 10,000 litres if–				
	(i) there is not a reticulated water supply; and				



12.	12.4 Development Standards				
Red	quirement/s	Assessment	Compliance		
	(ii) development is for – a. a single dwelling; or				
	b. a use with an equivalent population of not more than 10 people per day.				
A4		The site was an existing connection to a sewerage system which has been provided in accordance with the Water and Sewerage Industry Act 2008.	Complies with acceptable solution.		
	(ii) the development— a. a single dwelling; or b. provides for an equivalent population of not more than 10 people per day; or c. creates a total sewage and waste water flow of not more than 1,000l per day; and (iii) the site has capacity for on-site disposal of domestic waste water in accordance with AS/NSZ1547:2012 On-site domestic-				



12.4	12.4 Development Standards			
Red	quirement/s	Assessment	Compliance	
	management clear of defined building area or access strip.			
A5	A site or each lot on a plan of subdivision must be capable of draining and disposing of stormwater – (a) to a stormwater system provided in accordance with the Urban Drainage Act 2013; or (b) if stormwater cannot be drained to a stormwater system - (i) for discharge to a natural drainage line, water body, or watercourse; or (ii) for disposal within the site if –	connection to a stormwater		
	a. the site has an area of not less than 5000m²; b. the disposal area is not within any defined building area; c. the disposal area is not within any area required for the disposal of sewage; d. the disposal area is not within any access strip; and e. not more than 50% of the site is			
	impervious surface; and (iii) the development is for a single dwelling. 4.2 Dwelling density			

12.4.2 Dwelling density



12.4	12.4 Development Standards					
Red	quirem	ent/s	s		Assessment	Compliance
A1	– (a) b	oe n	area per dwell not less than nite has –		The site area per dwelling is 268.5m ² .	Relies on performance criteria.
			connection reticulated supply;	to a water		
		(ii)	connection reticulated system; and	to a sewer		
		(iii)	connection stormwater or	to a system;		
	(show Clau	e site is in a vn in the Tabl se, not less area for that lo	e to this than the		
12.4	4.3 Loc	atior	n and configur	ation of de	evelopment	
A1			of a building om a frontage		The adjoining lots contain dwellings that are setback	Complies with acceptable
	` '		ess than 4.5n ary frontage; a		from the Hepples Road frontage 1.2m on the lot to the north-east (17 Hepples	solution A1 (c).
	` ,		ess than 3.0m ndary frontage	•	Road) and 7.7m on the lot to the south-east (13 Hepples	
	τ ε t	han exist	ess than and i the setbacks ing building or immediate a ;	for any each of	Road). The proposed dwelling will be setback a minimum of 3.05m from the same frontage.	
	ìík		less than ing retained	,		
) k	ouild	accordance wing area showed plan; or	-		
) s	show Clau	e site abuts vn in the Tabl se, the ified for that ro	e to this setback		



12.4	1 Development Standards		
Rec	quirement/s	Assessment	Compliance
A2	All buildings must be contained within a building envelope determined by- (a) the applicable frontage setback;	The sections of the proposed dwelling along the north-western (side) and north-eastern (rear) boundary will be located outside the building	Relies on performance criteria.
	(b) if the site is in a locality shown in the Table to this Clause, not less than the setback distance specific from the feature specified;	envelope prescribed by the acceptable solution.	
	(c) projecting a line at an angle of 45° from the horizontal at a height of 3.0m above natural ground level at each side boundary and at a distance of 4.0m from the rear boundary to a building height of not more than 8.5m above natural ground level if walls are setback -		
	(i) not less than 1.5m from each side boundary; or		
	(ii) less than 1.5m from a side boundary if wall height is not more than 3.0m; and –		
	a.built against an existing wall of an adjoining building; or		
	b.the wall or walls -		
	i. have the lesser of a total length of 9.0m or one-third of the boundary with the adjoining land;		
	ii. there is no door or window in the wall of		



12.4 Development Standards Requirement/s	Assessment	Compliance
the building;		
iii. overshadowing does not result in -		
a. less than 2 hours of continuous sunlight to a required minimum private open space area in an adjacent dwelling between 9.00am and 3.00pm on 21st June; or		
b. a further reduction in continuous sunlight to a required minimum private open space area in an adjacent dwelling if already less than 2 hours between 9.00am and 3.00pm on 21st June; or		

12.4	12.4 Development Standards					
Red	quirement/s	Assessment	Compliance			
	(d) in accordance with any building envelope shown on a sealed plan.					
A3	Site coverage must -	Site coverage of the proposed dwelling has been	Complies with acceptable			
	(a) not be more than 50%; or(b) if the site is in a locality shown in the Table to this Clause, not more than the site coverage for that locality; and	calculated to be approximately 31%.	solution.			
	(c) not include any part of a site required for the disposal of sewage or stormwater; or					
	(d) be not more than any building area shown on a sealed plan.					
A4	A garage, carport or an external car parking area and any area for the display, handling, or storage of goods, materials or waste, must be located behind the primary frontage of a building.	No garage, carport, external parking areas are proposed. Waste storage areas are capable of being located behind the frontage setback of the new dwelling.	Complies with acceptable solution.			
A5	Total width of openings in the frontage elevation of a garage or carport (whether freestanding or part of any other building) must be the lesser of -	No garages or carports are proposed.	Not applicable.			
	(a) 6.0m; or					
	(b) half the width of the frontage.					
A6	If on a site at Boat Harbour, a building on the lower side of a road must be single storey on the road elevation.	The dwelling will be located on the lower side of Hepples Road and will be two storey on the road elevation.	Relies on acceptable solution.			
12.4	4.4 Visual and acoustic privacy for	residential development				
A1	A door or window to a habitable room, or any part of a balcony, deck, roof garden, parking space or carport of a building must –	The north-western, north- eastern and south-eastern walls of the first floor all	Complies with acceptable solution.			



12.4 Develo	oment Standards	12.4 Development Standards				
Requiremen	t/s	Assessment	Compliance			
mo	he finished floor level is re than 1.0m above cural ground level -	contain windows to habitable rooms. The north-eastern boundary				
(i)	be not less than 6.0m from any door, window, balcony, deck, or roof garden in a dwelling on the same site;	of the site adjoins the coastal reserve and constitutes the rear boundary. All habitable rooms windows on the first				
(ii)	be not less than 3.0m from a side boundary;	floor facing this boundary will be setback a minimum of 5m from the boundary.				
(iii)	be not less than 4.0m from a rear boundary; and	The north-western boundary of the site is a side boundary. All				
(iv)	if an internal lot, be not less than 4.5m from the boundary abutting a rear boundary of an adjacent frontage site; or	habitable room windows on the first floor facing this boundary will be within 3m of the boundary. The south- eastern wall of the adjoining dwelling does not contain				
, ,	ess than the setbacks in use A1(a) -	any windows. Windows of the adjoining dwelling are located on the north-				
(i)	be off-set by not less than 1.5m from the edge of any door or window in another dwelling;	eastern and south-western walls. Windows of the proposed dwelling will therefore be off-set a minimum of 1.5m from the				
(ii)	a have a window sill height of not less than 1.8m above finished floor level;	edge of any door or window of the adjoining dwelling. The south-eastern boundary of the site is a				
(iii)	have fixed and durable glazing or screening with a uniform transparency of not more than 25% in that part of a door or window less than 1.7m above finished floor level; or	side boundary. The south- eastern elevation of the first floor will contain one habitable room window which corresponds with the master bedroom. This window will have a minimum sill height of 1.7m above finished floor level.				
(iv)	have fixed and durable external screen other than vegetation of not less than 1.8m height above the finished floor	The north-eastern and south-eastern elevations of the deck will include a screening structure that will have a minimum height of				



12.	12.4 Development Standards				
Red	quirement/s	Assessment	Compliance		
	level and with a uniform transparency of not more than 25% located for the full width of the door, window, balcony, deck, roof garden, parking space, or carport.	1.7m above finished floor level and a minimum transparency of 25%.			
A2	An access strip or shared driveway, including any pedestrian pathway and parking area, must be separated by a distance of not less than 1.5m horizontally and 1.5m vertically from the door or window to a dwelling or any balcony, deck, or roof garden in a dwelling.	The site does not contain an access strip or shared driveway.	Not applicable.		
12.	4.5 Private open space for resident	ial use			
A1	Each dwelling must provide private open space — (a) if a dwelling with a floor level of not more than 2.5m above finished ground level, a ground level area - (i) located adjoining the rear or side of the dwelling; (ii) accessible from the dwelling; (iii) of not less than 25m²; (iv) with a minimum dimension of 4.0m; (v) on a single level; and (vi) with a gradient of not more than 1 in 10; and (b) if a dwelling with a floor level of more than 2.5m above finished ground level, as an alternative to a ground level area, a private balcony, deck, terrace or roof garden —	An existing levelled area of private open space will remain to the north-east of the dwelling between the dwelling and rear boundary. It has a minimum area of 25m² and minimum horizontal dimensions of 4m. It is accessible from the ground floor of the dwelling.	Complies with acceptable solution.		



12.4	12.4 Development Standards				
Rec	juirement/s	Assessment	Compliance		
	(i) of not less than 25m²; (ii) with a minimum				
	dimension of 4.0m; and				
	(iii) accessible from the dwelling.				
A2	The required minimum private open space area must be capable of receiving at least 3 hours of sunlight between 9.00am and 3.00pm on 21st June.	The designated area of private open space is located to the north-east of the dwelling adjacent to the coastal reserve. It is therefore capable of receiving a minimum of 3 hours of sunlight between 9:00am and 3:00pm on 21st June.	Complies with acceptable solution.		
A3	Unless there is a ground level private open space area directly accessible at grade to a shared driveway or pedestrian pathway, each dwelling in a multiple dwelling development must have access to a waste storage area — (a) located behind the applicable frontage setback; (b) of not less than 1.5m² per dwelling; (c) screened to view from the frontage and any dwelling by a wall of height not less than 1.2m above finished	Multiple dwelling development is not proposed.	Not applicable.		
	ground level; and (d) not less than 6.0m from a window, door, balcony, deck, roof garden or private open space area of a dwelling.				
12.4	1.6 Frontage fences				
A1	The height of a fence, including any supporting retaining wall, on a frontage or within a frontage setback must be –	No frontage fences are proposed.	Not applicable.		

12.4	4 Development Standards		
Red	quirement/s	Assessment	Compliance
	(a) not more than 1.2m if the fence is solid; or		
	(b) not more than 1.8m provided that part of the fence above 1.2m has openings that provide a uniform transparency of not less than 30%.		
12.4	1.7 Setback of development for ser	nsitive use	
A1	A building containing a sensitive use must be contained within a building envelope determined by –	zone listed within Table	Not applicable.
	(a) the setback distance from the zone boundary as shown on the Table to this clause; and		
	(b) projecting upward and away from the zone boundary at an angle of 45° above the horizontal from a wall height of 3.0m at the setback distance from the zone boundary.		
A2	Development for a sensitive use must be not less than 50m from – (a) a major road identified in the Table to this clause;	The proposed dwelling will be setback greater than 50m from a major road, railway (including land designated for future road and rail purposes) and	Complies with acceptable solution.
	(b) a railway;	proclaimed wharf area.	
	(c) land designated in the planning scheme for future road or rail purposes; or		
	(d) a proclaimed wharf area.		

3.2 Change in Ground Level Code

Cut is required directly below the south-western section of the first floor level of the existing dwelling between the ground floor level and existing walkway. The cut will have a maximum depth of approximately 2.3m at the south-western end and will taper to existing ground level at the north-eastern end. The cut will be located 1m from the north-western boundary, 3m from the frontage boundary and 2.9m from the south-



eastern boundary. The cut will be supported by a retaining wall located within 1m of the north-western boundary and 3m from the frontage boundary. The retaining wall will have a maximum height of approximately 2.2m. The cut does not satisfy the exemption in Clause E4.4.1 (b) (i) and (ii). Assessment against the Code is therefore required.

E4.	E4.6 Development Standards				
Red	quiremen	t/s	Assessment	Compliance	
E4.0	6.1 Chang	ge in existing ground leve	l or natural ground level		
A1	Env or Ma	be on land within the vironmental Living zone the Environmental nagement zone;	(a) the site is zoned Low Density Residential.(b) the cut is required to provide a construction site for a building and associated structures.	Complies with acceptable solution.	
	(i)	required to - provide a construction site for buildings and structures; facilitate vehicular	(c) all surface water will be collected from hard impervious surfaces and discharged to the public stormwater system.		
	. ,	access; mitigate exposure to a natural or environmental hazard;	(d) the cut will be supported by an engineered retaining wall. The retaining wall will be located along the		
		facilitate provision of a utility; assist the consolidation or intensification of development; or	exposed face of the cut and backfilled. The retaining wall will be designed to bear load		
		assist stormwater management;	from adjoining properties to ensure existing buildings on adjacent land remain stable.		
	of wat	result in a modification surface stormwater ter flow to increase – surface water drainage	(e) the retaining walls will include a drainage system at the base of the wall that will collect		
	(ii)	onto adjacent land; pooling of water on the site or on adjacent land; or	intersected ground water and discharge it to the public stormwater system.		
	(iii)	the nature or capacity of discharge from land upstream in a natural or artificial drainage channel;	(f) the retaining wall system will include an ag-pipe wrapped in geotextile fabric with a permeable drainage layer above. This will catch and filter		



E4.6 Development Standards		
Requirement/s	Assessment	Compliance
(d) not destabilise any existing building or increase the requirements for construction of any potential building on adjacent land;	sediments from water before it is discharged to the public stormwater system once it becomes operational. Soil and water	
sediments and other contaminants during each of the site preparation, construction and rehabilitation phase in accordance with Soil and Water Management on Building and Construction Sites 2009; (g) not require a retaining or support structure that would result in an area of influence within the boundary of adjacent land;	management plans will be implemented during the construction to minimise the release of sediments from the site. (g) the cut will be supported by retaining walls. Bearing pressure exerted on the ground at the surface of the cut and the retaining wall will come from the adjoining property to the northwest and Hepples Road to the south-west. The footings of the retaining wall will be engineered to ensure bearing pressure from adjacent land will not impact the structural integrity of the wall.	
and (h) not encroach upon or expose, disturb, or reduce cover over an underground utility to less than 1.0m unless the relevant regulatory entity has advised – (i) it is satisfied the cut or fill will not result in harm to the utility; and (ii) any condition or requirement it determines are appropriate to protect the utility.	The cut and associated retaining wall will not impact the structural integrity of a retaining wall on adjacent land to the north-west and south-west. (h) the cut will not expose, disturb, encroach upon, or reduce cover over the sewerage pipe located within the easement parallel to the north-western boundary of the site.	



3.3 Hazard Management code

E6.	5 Use Standards			
Requirement/s		Assessment	Compliance	
E6.	5.2 Use likely to be exposed to a n	atural hazard		
A1	If a use is on land within an area of risk from exposure to a natural hazard as shown on a map forming part of this planning scheme - (a) use must not be for a critical use, a hazardous use, or a vulnerable use; (b) use must not be residential use if the level of risk is medium or higher; and (c) a hazard risk assessment must demonstrate a tolerable level of risk can be achieved and maintained for the nature and duration of the use.		in accordance with clause 7.4.2(b) of the	

E	E6.6 Development Standards				
F	Requirement/s		Assessment	Compliance	
E	6.0	6.2 Development on land exposed	to a natural hazard		
A	\1	If the site is within an area of risk shown on a natural hazard map forming part of this planning scheme – (a) a hazard risk assessment must determine - (i) there is an insufficient increase in risk to warrant any specific hazard reduction or protection measure; or (ii) a tolerable level of risk can be achieved for the type, form, scale and duration of the development; and	has determined that there is		



E6.6 Development Standards		
Requirement/s	Assessment	Compliance
(b) if a hazard risk assessment established need to involve land on another title for hazard management consistent with the objective, the consent in writing of the owner of that land must be provided to enter into a Part 5 agreement to be registered on the tile of the land and providing for the effected land to be managed in accordance with recommendations for hazard management.		

3.4 Traffic Generating Use and Parking Code

E9.5 Use Standards			
Requirement/s		Assessment	Compliance
E9.	5.1 Provision for parking		
A1	Provision for parking must be - (a) the minimum number of onsite vehicle parking spaces must be in accordance with the applicable standard for the use class as shown in the Table to this Code.	Table E9.1 requires a dwelling in a zone other than the General Residential zone to provide 2 car parking spaces. The existing dwelling does not provide any on-site parking spaces. The site is unable to provide feasible parking spaces due to the topographical constraints. The proposal is for a replacement dwelling and will not provide parking. It will not increase the demand for parking spaces. The application therefore does not affect issues dealt with by the code directly. The Code is not considered applicable to the application	Not applicable.



E9.5 Use Standards		
Requirement/s	Assessment	Compliance
	in accordance with clause 7.4.2(b) of the Scheme.	

3.5 Water and Waterways Code

E10	E10.6 Development Standards					
Requirement/s Assessment			Compliance			
10.6	6.2 Development in in a shoreline a	area				
A1	There is no acceptable solution.	There is solution.	not	acceptable	Relies performan criteria.	on ice



4.0 Performance Criteria Assessment

The proposed development relies on several performance criteria which are addressed below.

4.1 Clause 12.4.1 Suitability of a site or lot for use or development - Performance Criteria P1

12.4.1 Suitability of a site or lot for use or development

Objective:

The minimum properties of a site and of each lot on a plan of subdivision are to -

- (a) provide a suitable development area for the intended use;
- (b) provide access from a road; and
- (c) make adequate provision for a water supply and for the drainage and disposal of sewage and stormwater.

or sewage and stormwater.	
Acceptable Solutions	Performance Criteria
A1	P1
A site or each lot on a plan of subdivision must –	A site or each lot on a plan of subdivision must -
 (a) have an area of - (i) not less than 500m² excluding any access strip; or 	(a) be of sufficient area for the intended use or development without likely constraint or interference for –
(ii) if in a locality shown in the Table to this clause, not less than the site area shown for that locality; and	(i) erection of a building if required by the intended use;(ii) access to the site;
(b) contain a building area of not less than 10.0m x 15.0m -	(iii) use or development of adjacent land;
(i) clear of any applicable setback from a frontage, side or rear boundary;	(iv) a utility; and (v) any easement or lawful entitlement for access to other land; and
(ii) clear of any applicable setback from a zone boundary;	(b) if a new residential lot, be orientated to maximise opportunity for solar access to a building area.
(iii) clear of any registered easement;	

(iv)	clear of any registered right of way benefitting other land;
(,,)	aloan of any rootriction

- (v) clear of any restriction imposed by a utility;
- (vi) not including an access strip;
- (vii) accessible from a frontage or access strip; and
- (viii) if a new residential lot, with a long axis within the range 30° east of north and 20° west of north.

Response

The site has an area of 268.5m² and is unable to contain a building area of not less than 10m by 15m in a location that is clear of applicable side and rear setbacks. Assessment against the performance criteria is therefore required.

Performance Criteria Assessment

The site is of sufficient area to support the replacement dwelling without likely constrain or interference to adjacent land, public infrastructure and the environment having regard to the following:

- (a) the site is capable of providing a building area suitable for residential use which is demonstrated by the presence of the existing dwelling;
- (b) the established pedestrian access from Hepples Road will be retained;
- (c) the proposed development will not substantially alter the established relationship with existing residential development on adjacent land to the northwest and south-east. The relationship is characterised by small lots that contain compact single dwelling development proximate to side boundaries;
- (d) the site will not constrain or interfere with a utility;
- (e) the building area of the existing dwelling and for the replacement dwelling is clear of the registered easement which is 1m in width and runs parallel to the north-western boundary; and
- (f) no new residential lots will be created.



The application complies with the performance criteria.

4.2 Clause 12.4.2 Dwelling density - Performance Criteria P1

12.4.2 Dwelling density

Residential dwelling density is to -

- (a) make efficient use of land for housing;
- (b) optimise utilities and community services; and
- (c) be consistent with any constraint on suitability of the land for residential use.

Acceptable Solutions	Performance Criteria	
A1	P1	
The site area per dwelling must – (a) be not less than 500m² if the site has –	The number of dwellings on a site must be consistent with the capability of the land for residential use in terms of –	
(i) connection to a reticulated water supply;	(a) a suitable building area;(b) access from a road;	
(ii) connection to a reticulated sewer system; and	(c) provision of a water supply;	
(iii) connection to a stormwater system; or	(d) disposal of sewage;(e) disposal of stormwater; and	
(b) if the site is in a locality shown in the Table to this Clause, not less than the site area for that locality.	(f) a tolerable level of risk from a natural hazard.	

Response

The site area per dwelling is 268.5m². Assessment against the performance criteria is therefore required.

Performance Criteria Assessment

The proposal is for single dwelling use and development. The site is capable of supporting a single dwelling having regard to the following:

- (a) the site is capable of providing a building area suitable for residential use which is demonstrated by the presence of the existing dwelling;
- (b) the site has 18m frontage to Hepples Road. The established pedestrian access to the site from Hepples Road will be retained;



- (c) the site has an existing connection to a water supply;
- (d) the site has an existing connection to a sewage system;
- (e) the site has an existing connection to a stormwater discharge point;
- (f) the hazard risk assessment has determined that there is an insufficient increase in risk to warrant specific hazard reduction or protection measure with respect to landslip hazards.

The application complies with the performance criteria.

4.3 Clause 12.4.3 Location and configuration of development - Performance Criteria P2

12.4.3 Location and configuration of development

Objective:

The location and configuration of development is to –

- (a) be consistent with land capability;
- (b) provide a consistent separation between the development area on adjacent sites and between development and a road;
- (c) provide consistency in the apparent scale, bulk, massing, and proportion of adjacent buildings;
- (d) provide sufficient site area for open space, utilities, and vehicle parking;
- (e) provide for the facade of a residential building to remain the dominant architectural element in the streetscape; and
- (f) separate adjacent buildings to provide reasonable opportunity for daylight and sunlight to habitable rooms and to private open space areas.

Acceptable Solutions	Performance Criteria		
A2	P2		
All buildings must be contained within a building envelope determined by-	Building height and location of a building in relation to a frontage and site boundaries must -		
(a) the applicable frontage setback;(b) if the site is in a locality shown in the Table to this Clause, not less than the setback distance specific from the feature specified;	(a) minimise likelihood for overshadowing of a habitable room or a required minimum area of private open space in any adjacent dwelling;		



- (c) projecting a line at an angle of 45° from the horizontal at a height of 3.0m above natural ground level at each side boundary and at a distance of 4.0m from the rear boundary to a building height of not more than 8.5m above natural ground level if walls are setback -
 - (i) not less than 1.5m from each side boundary; or
 - (ii) less than 1.5m from a side boundary if wall height is not more than 3.0m; and –
 - a. built against an existing wall of an adjoining building; or
 - b. the wall or walls -
 - i. have the lesser of a total length of 9.0m or one-third of the boundary with the adjoining land;
 - ii. there is no door or window in the wall of the building; and
 - iii. overshadowing does not result in
 - a. less than 2 of hours continuous sunlight to required minimum private open space area in an adjacent dwelling between 9.00am and 3.00pm on 21st June; or

- (b) minimise the apparent scale, bulk, massing and proportion relative to any adjacent building;
- (c) be consistent with the streetscape;
- (d) respond to the effect of the slope and orientation of the site; and
- (e) provide separation between buildings to attenuate impact.

- further b. a reduction continuous sunlight to а required minimum private open space area in an adjacent dwelling already less than 2 hours between 9.00am and 3.00pm on 21st June; or
- (d) in accordance with any building envelope shown on a sealed plan.

Response

The north-western wall of the replacement dwelling will be setback between 1m and 1.3m from the boundary. The wall will have a maximum length of 8.9m. Upper sections of the wall and part of the roof extend outside the 45° envelope on this side. The north-eastern wall of the dwelling and sections of the deck will be within 4m of the rear boundary.

Assessment against the performance criteria is therefore required.

Performance Criteria Assessment

The height and location of the proposed replacement dwelling in relation to the frontage and site boundaries will be appropriate with respect to minimising impacts on the amenity of adjacent residential uses and compatibility with the built form and character of the area, having regard to the following:

(a) the replacement dwelling will be located to the south-east of the adjoining dwelling to the north-west. The south-eastern wall of the adjoining dwelling is built to the boundary and does not contain any windows or other openings. Likelihood for overshadowing to occur to habitable room windows and private open space of the adjoining dwelling to the north-west is therefore minimised by these factors;

The replacement dwelling will be contained within the prescribed building envelope with respect to the south-eastern boundary. The degree of any overshadowing to the adjacent dwelling to the south-east is therefore assessed as being acceptable.

The rear boundary of the site adjoins the Boat Harbour beach coastal reserve and is therefore not adjacent to residential use and development.

(b) the bulk, massing and proportion of the replacement dwelling will be similar to the existing dwelling to be demolished. The primary difference between the existing dwelling and replacement dwelling will be the inclusion of a gable roof from a skillion roof which will increase the roof height from 5.6m to 7.1m (+1.5m). The footprint of the replacement will be similar to the two dwellings to the southeast on the same side as Hepples Road. The footprint will be smaller than the adjacent dwelling to the north-west and other dwellings further along.

The apparent scale, bulk and massing of the replacement dwelling relative to adjacent dwellings will be minimised by:

- keeping a similar building footprint, wall height and appearance as the
 existing dwelling to be replaced which will minimise the perceived spatial
 change from adjacent dwellings and within the streetscape and along the
 coastal reserve;
- retaining similar (if not the same) separation distances from adjacent dwellings to the north-west and south-east; and
- aligning the gable of the roof north-east to south-west which will ensure
 the highest point of the roof recesses into the site relative to side
 boundaries which will assist in minimising the apparent scale and form of
 the building when viewed from adjacent dwellings.
- (c) the setbacks and height of the replacement dwelling will be compatible with surrounding residential development. It has therefore been designed having regard to established streetscape qualities;
- (d) the building area will have a level surface and will not be impacted by topographical constraints;
- (e) the replacement dwelling will retain established separation distances relative to adjacent and nearby dwellings.

The application complies with the performance criteria.

4.4 Clause 12.4.3 Location and configuration of development - Performance Criteria P6

12.4.3 Location and configuration of development

Objective:

The location and configuration of development is to -

- (a) be consistent with land capability;
- (b) provide a consistent separation between the development area on adjacent sites and between development and a road;



- (c) provide consistency in the apparent scale, bulk, massing, and proportion of adjacent buildings;
- (d) provide sufficient site area for open space, utilities, and vehicle parking;
- (e) provide for the facade of a residential building to remain the dominant architectural element in the streetscape; and
- (f) separate adjacent buildings to provide reasonable opportunity for daylight and sunlight to habitable rooms and to private open space areas.

Acceptable Solutions	Performance Criteria
A6	P6
If on a site at Boat Harbour, a building on the lower side of a road must be single storey on the road elevation.	If on a site at Boat Harbour a building on the lower side of a road must be located within the site and be of a mass and height that does not result in an unreasonable loss of outlook from the immediately adjacent site on the high side of the road.

Response

The replacement dwelling will be located on the lower side of Hepples Road and will be two storeys. Assessment against the performance criteria is therefore required.

Performance Criteria Assessment

The existing ground level of the building area is situated approximately 7m below the pavement of Hepples Road at the high side of the road. The replacement dwelling will have a building height of 7.1m which is measured to the ridge of the gabled roof. The building will therefore marginally extend above the surface of Hepples Road at certain points.

The immediately adjacent site on the high side of Hepples Road is currently vacant. Its natural ground level is approximately 1m above the pavement of Hepples Road at the frontage. It continues to rise toward the rear boundary where natural ground level is approximately 10m above the pavement of Hepples Road.

Accordingly, the height and mass of the proposed dwelling will not result in an unreasonable loss of outlook from the immediately adjacent site on the high side of Hepples Road when considering the topography of the adjacent site and extent of the replacement dwelling that will extend above the pavement of Hepples Road.

The application complies with the performance criteria.



4.5 Clause E10.6.2 Development in a shoreline area - Performance Criteria P1

E10.6.2 Development in a shoreline area

Objective:

Coastal waters and the shoreline area are protected against likely impact of development within 30m of or located in, over, on or under the coastal waters or shoreline area on economic, ecological, scenic, cultural, and recreation values, and for processes of the coast while facilitating use dependent for operational efficiency on a coastal location.

Acceptable Solutions	Performance Criteria
A1	P1
There is no acceptable solution.	Development must –
	(a) be required to locate in, over, on or under the shoreline, sea or tidal waters for operational efficiency;
	(b) avoid unreasonably or unnecessarily impact on existing or potential access by the public to shoreline land or waters;
	(c) minimise impact on scenic quality of the sea-shore area;
	(d) minimise impact on amenity or aesthetic appearance of the seashore area as a result of –
	(i) nature and operational characteristics of the development;
	(ii) location;
	(iii) bulk, size, and overall built form of any building or work;
	(iv) overshadowing; or
	(v) obstruction of views from a public place; and
	(e) minimise immediate or cumulative adverse effect for –

(i)	tidal,	wave,	current,	or
	sedim	ent	moven	nent
	proces	sses;		

- (ii) coastal landforms, seabed, and other geomorphic features, including sand dunes and mobile landforms;
- (iii) vulnerability to erosion and recession;
- (iv) natural cycles of deposition and erosion;
- (v) conservation of biodiversity and marine habitat, including during critical lifecycle stages of individual and migratory species;
- (vi) drainage from a water course, wetland, ground water, flood, stormwater, or tidal water;
- (vii) coastal water quality;
- (viii) likely interference or constraint on use of public areas;
- (ix) any scientific, architectural, aesthetic, historic of special cultural value;
- (x) exposure to or increased risk from a natural hazard, including sea level rise, storm surge, or inundation as a result of climate change;
- (xi) coastal protection and rehabilitation works required to address erosion, instability, regression, or inundation;
- (xii) collection, treatment, and disposal of waste, including bilge waters and excavated or dredged sediment;

(xiii)	economic activity dependent for operational efficiency on a sea-shore location;
(xiv)	public safety and emergency services;
(xv)	marine navigation and communication systems;
(xvi)	safety of recreational boating; and
(xvii)	be consistent with the current edition of Tasmanian Coastal Works Manual DPIPWE 2011.

Response

The site is located within 30m of the high water mark of a shoreline to an ocean. There is not acceptable solution. The application therefore relies on the performance criteria.

Performance Criteria Assessment

The shoreline area adjacent to the site will be protected against potential adverse impacts of the proposed development, having regard to the performance criteria, on the following basis:

- (a) all development will be located a minimum of 22m from the mapped mean high water mark of Boat Harbour Beach and will be contained entirely within the boundaries of the site. The development will therefore not be located in, over, on or under the shoreline;
- (b) the proposed development will not impact on the existing public access to the beach in proximity to the site which is located approximately 35m to the southeast;
- (c) and (d) Boat Harbour is a small beachside settlement characterised by relatively high density development along the foreshore of Boat Harbour beach. The pattern of development along Boat Harbour beach between 276 Port Beach Road and 9 Hepples Road is particularly compact, being characterised by small lot sizes with an average size of 350m² and down to 188m². As a result of the smaller lot sizes, buildings are typically located close to the foreshore and close to lot boundaries and adjoining buildings.

The replacement dwelling will be located within a similar footprint as the existing dwelling and will be of a form and scale that that will be consistent with existing buildings located along the foreshore. The setback from the foreshore boundary on the site established by the existing building will not be significantly altered by



the replacement dwelling. Further the proposed setback will be greater than the setback of buildings relative to the foreshore boundary on adjoining and nearby lots to the north.

The replacement dwelling will be located on the lower side of Hepples Road and will be constructed to a height that is equal to the surface level of Hepples Road. This will ensure views from Hepples Road and other public areas that are on the high side of the site are not obstructed.

Accordingly, the replacement dwelling will be consistent with the established scenic quality, amenity and aesthetic appearance of the sea-shore area.

(e) the replacement dwelling will be located within a similar footprint as the existing dwelling. The footprint is located approximately 22m from the mean high water mark of Boat Harbour Beach. The replacement dwelling will not introduce a new use or substantially intensify the existing residential use. The proposed development is therefore not expected to result in immediate or cumulative adverse effects for coastal processes and functions, vulnerability to erosion and recession, or coastal protection. No changes to existing coastal water quality is expected as a result of the proposed development. The site does not contain any significant natural values or marine habitat. Further, the proposed development will not interfere or constrain on use of the public foreshore, safety and emergency services, marine navigation and communication systems, and recreational boating.

The application complies with the performance criteria.



5.0 Conclusion

The proposed development involves the demolition of an existing dwelling, construction of a replacement dwelling and construction of new retaining walls. It relates to land located at 13 and 15 Hepples Road, Boat Harbour which is subject to the Low Density Residential zone.

The preceding assessment has determined that the proposed use and development complies with the applicable Scheme standards in the Low Density Residential zone and relevant code provisions, including the following performance criteria:

- Clause 12.4.1 Suitability of a site or lot for use or development -Performance Criteria P1;
- Clause 12.4.2 Dwelling density Performance Criteria P1;
- Clause 12.4.3 Location and configuration of development Performance Criteria P2 and P6; and
- Clause E10.6.2 Development in a shoreline area Performance Criteria P1.

It is therefore submitted that a discretionary permit can be issued for the proposed use and development in accordance with Section 51 and 57 of the *Land Use Planning and Approvals Act 1993*.

Appendix A

Certificate of Title



RECORDER OF TITLES



Issued Pursuant to the Land Titles Act 1980

OWNER G.L. & M.J. TREVERTON , J.G. & C.A. QUILLIAM AND THE CROWN

FOLIO REFERENCE C.T.56030-7 & 8

GRANTEF

PART OF LOT 6411 GTD. TO

JOSEPH THOMAS ALEXANDER & WHOLE OF

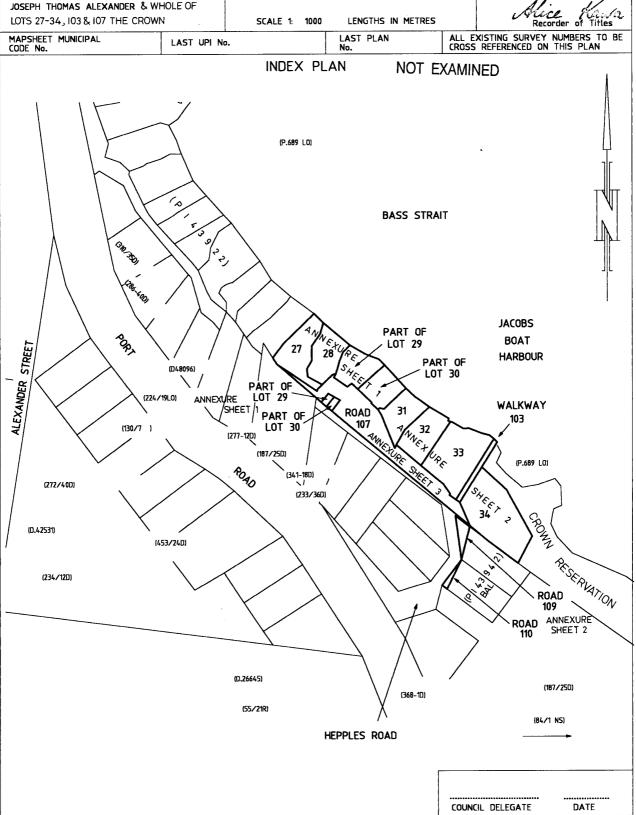
PLAN OF SURVEY
BY SURVEYOR CRAIG B. ROGERSON
120 CAMBRIDGE ROAD ROSNY PARK 7018
PH 6244-6256 FAX 6244-6221 MOB. 0418-120-796

LAND DISTRICT OF WELLINGTON PARISH OF SHEKLETON

REGISTERED NUMBER P143923

APPROVED -3 JUN 2005

Recorder of Titles



Search Date: 22 May 2018

Search Time: 12:22 PM

Volume Number: 143923

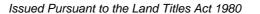
Revision Number: 01

Page 1 of 4



RESULT OF SEARCH

RECORDER OF TITLES





SEARCH OF TORRENS TITLE

VOLUME	FOLIO
143923	32
EDITION 4	DATE OF ISSUE 27-Aug-2007

SEARCH DATE : 22-May-2018 SEARCH TIME : 12.22 PM

DESCRIPTION OF LAND

Parish of SHEKLETON Land District of WELLINGTON Lot 32 on Plan 143923 (Section 27A of the Land Titles Act.) Derivation: Whole of Lot 32 on Plan 143923 Gtd. to The Crown

SCHEDULE 1

C572360 TRANSFER to GRANT ANTHONY MEDWIN and DEAN ROBERT MEDWIN as tenants in common in equal shares Registered 02-Nov-2006 at noon

SCHEDULE 2

C617489	Land is limited in depth to 15 metres, excludes
	minerals and is subject to reservations relating to
	drains sewers and waterways in favour of the Crown
C572360	Land is limited in depth to 15 metres, excludes
	minerals and is subject to reservations relating to
	drains sewers and waterways in favour of the Crown
C572360	FENCING PROVISION in Transfer
C617576	EASEMENTS set forth in Order
C979804	Proclamation: The above land is affected by Landslip
	(Wynyard) Order 1975 (Statutory Rules 1975 No. 286).
	Registered 10-Dec-2010 at noon

UNREGISTERED DEALINGS AND NOTATIONS

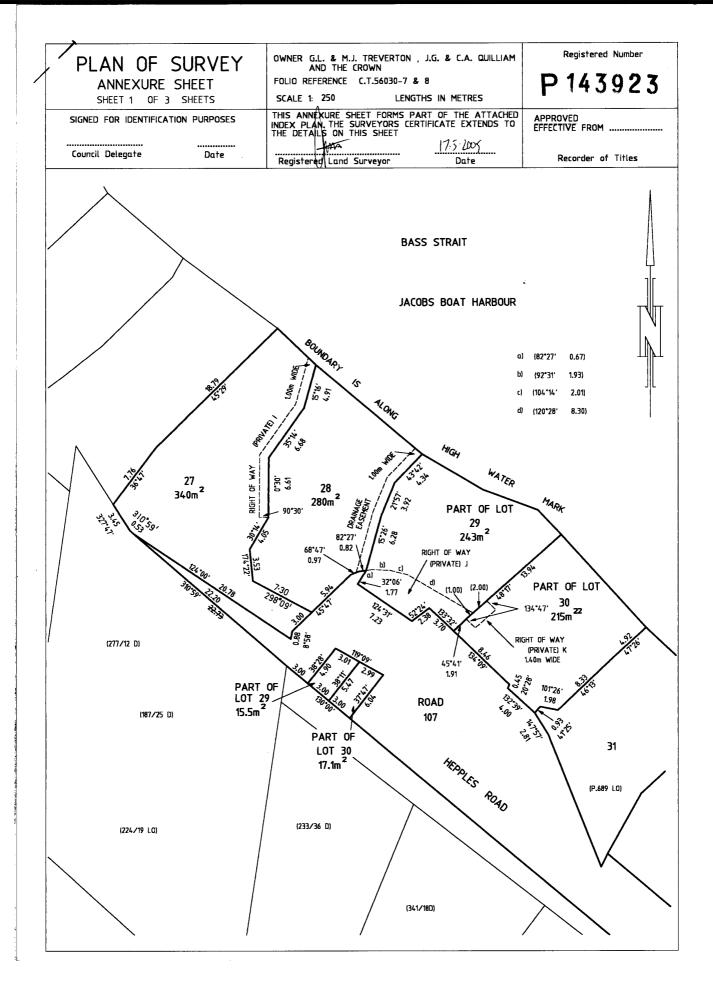
No unregistered dealings or other notations



RECORDER OF TITLES



Issued Pursuant to the Land Titles Act 1980



Search Date: 22 May 2018

Search Time: 12:22 PM

Volume Number: 143923

Revision Number: 01

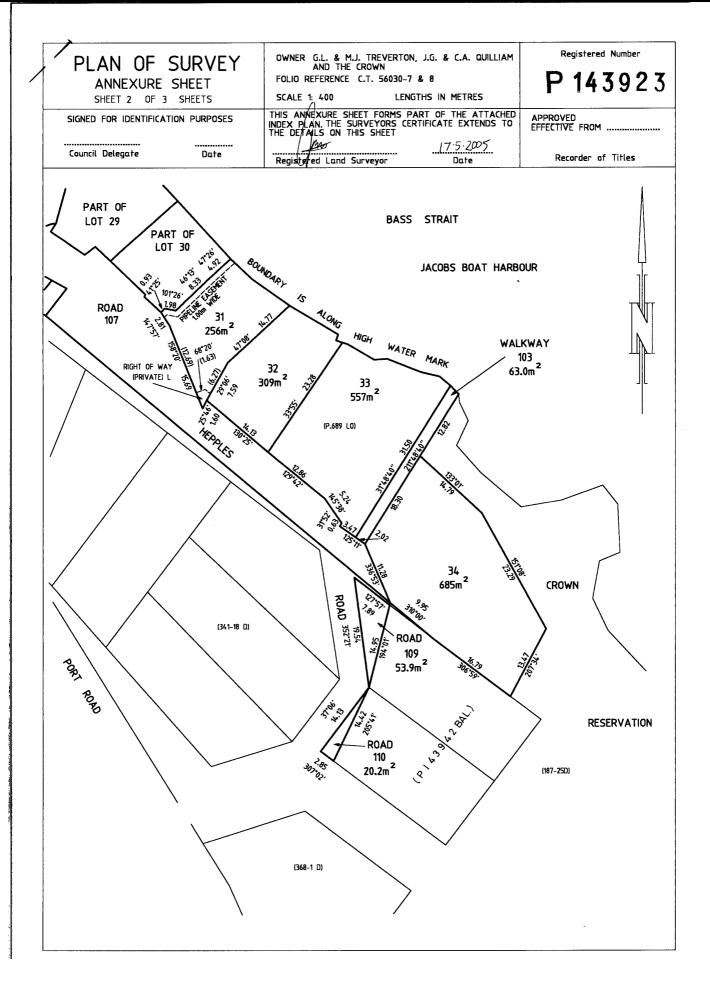
Page 2 of 4



RECORDER OF TITLES



Issued Pursuant to the Land Titles Act 1980



Search Date: 22 May 2018

Search Time: 12:22 PM

Volume Number: 143923

Revision Number: 01

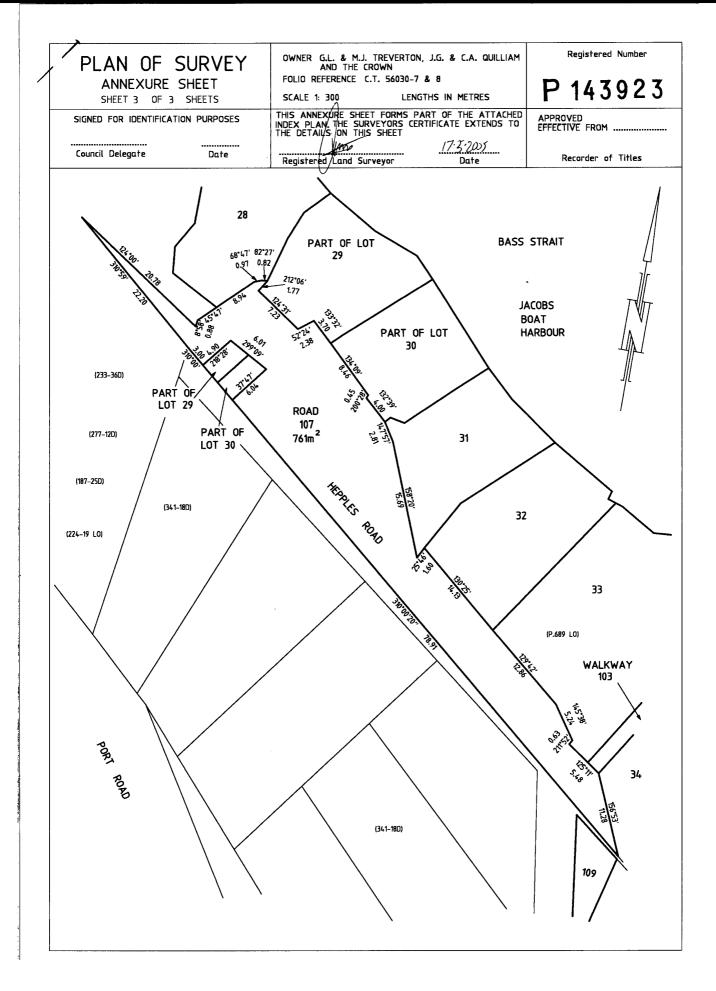
Page 3 of 4



RECORDER OF TITLES



Issued Pursuant to the Land Titles Act 1980



Search Date: 22 May 2018

Search Time: 12:22 PM

Volume Number: 143923

Revision Number: 01

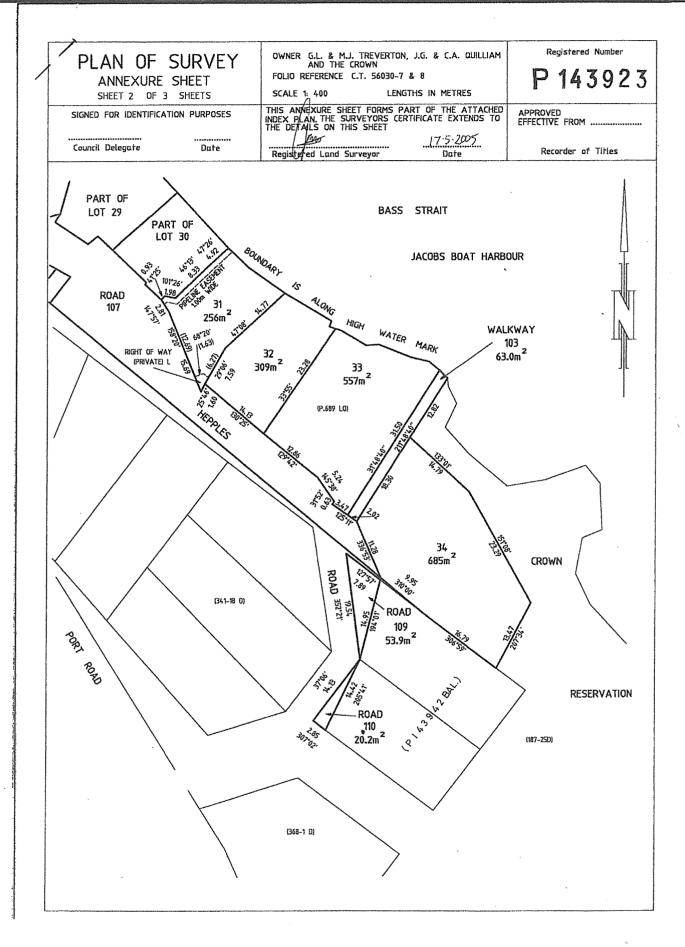
Page 4 of 4



RECORDER OF TITLES







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Search Time: 12:43 PM

Volume Number: 143923

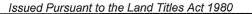
Revision Number: 01

Page 3 of 4



RESULT OF SEARCH

RECORDER OF TITLES







SEARCH OF TORRENS TITLE

VOLUME	FOLIO
143923	31
EDITION	DATE OF ISSUE
5	10-Jan-2013

SEARCH DATE : 23-Oct-2017 SEARCH TIME : 12.43 PM

DESCRIPTION OF LAND

Parish of SHEKLETON Land District of WELLINGTON Lot 31 on Plan 143923 (Section 27A of the Land Titles Act.) Derivation: Whole of Lot 31 on Plan 143923 Gtd. to The Crown

SCHEDULE 1

C742596 TRANSFER to CLARENCE JOHN KELLY and ROBYN SUZANNE KELLY Registered 08-Jan-2007 at noon

SCHEDULE 2

C617489	Land is limited in depth to 15 metres, excludes
	minerals and is subject to reservations relating to
	drains sewers and waterways in favour of the Crown
C742596	Land is limited in depth to 15 metres, excludes
	minerals and is subject to reservations relating to
	drains sewers and waterways in favour of the Crown
C742596	FENCING PROVISION in Transfer
C617576	EASEMENTS set forth in Order
C979804	Proclamation: The above land is affected by Landslip
	(Wynyard) Order 1975 (Statutory Rules 1975 No. 286).
	Registered 10-Dec-2010 at noon

UNREGISTERED DEALINGS AND NOTATIONS

No unregistered dealings or other notations



RECORDER OF TITLES

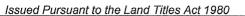




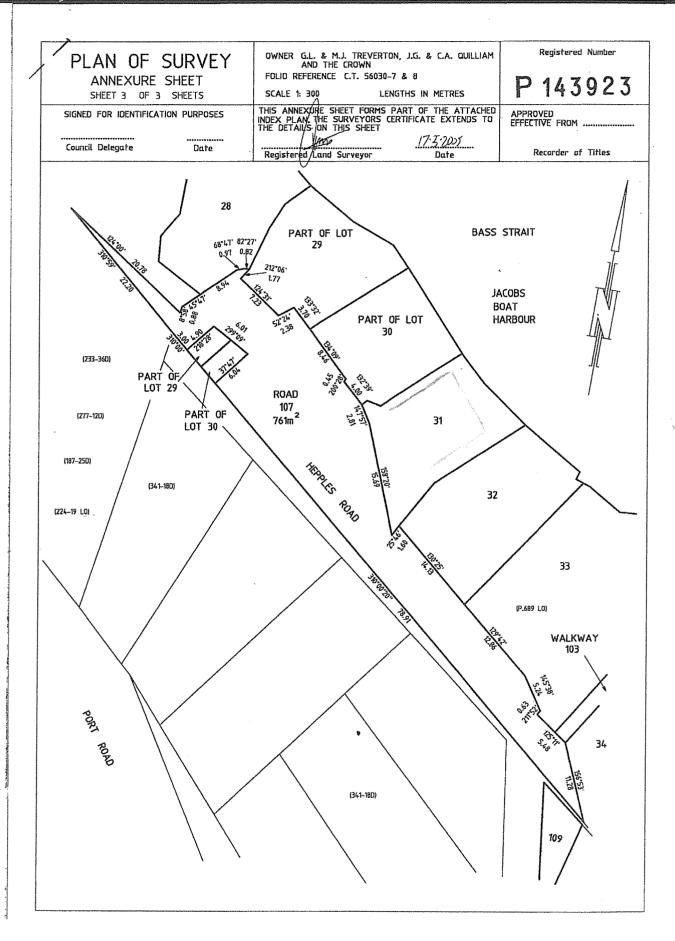
REGISTERED NUMBER PLAN OF SURVEY
BY SURVEYOR CRAIG B. ROGERSON
120 CAMBRIDGE ROAD ROSNY PARK 7018
PH 6244-6256 FAX 6244-6221 MUB. 0418-120-796
LOCATION OWNER G.L. & M.J. TREVERTON , J.G. & C.A. QUILLIAM AND THE CROWN P143923 FOLIO REFERENCE C.T.56030-7 & 8 LAND DISTRICT OF WELLINGTON GRANTEE PARISH OF SHEKLETON PART OF LOT 6411 GTD. TO JOSEPH THOMAS ALEXANDER & WHOLE OF LOTS 27-34, 103 & 107 THE CROWN SCALE 1: 1000 LENGTHS IN METRES ALL EXISTING SURVEY NUMBERS TO BE CROSS REFERENCED ON THIS PLAN MAPSHEET MUNICIPAL CODE No. LAST PLAN LAST UPI No. INDEX PLAN NOT EXAMINED (P.689 LO) BASS STRAIT GR AD **JACOBS** PART OF OR, BOAT LOT 29 STREET 27 HARBOUR PART OF (D48096) LOT 30 ALEXANDER PART OF LOT 29 ANNEXURE LOT 2. (224/19LO) WALKWAY ROAD 103 107 1130/7] **LOT 30** MEX 32 (277-120) 33 (187/250) OPE. (P.689 LO) POAD (272/400) SHEET (233/360) (D.42531) (453/24D) RESERVATION (234/120) ROAD 109 ROAD ANNEXURE (D.Z6645) (187/25D) (368-1D) (55/21R) 184/1 NS) HEPPLES ROAD COUNCIL DELEGATE DATE



RECORDER OF TITLES

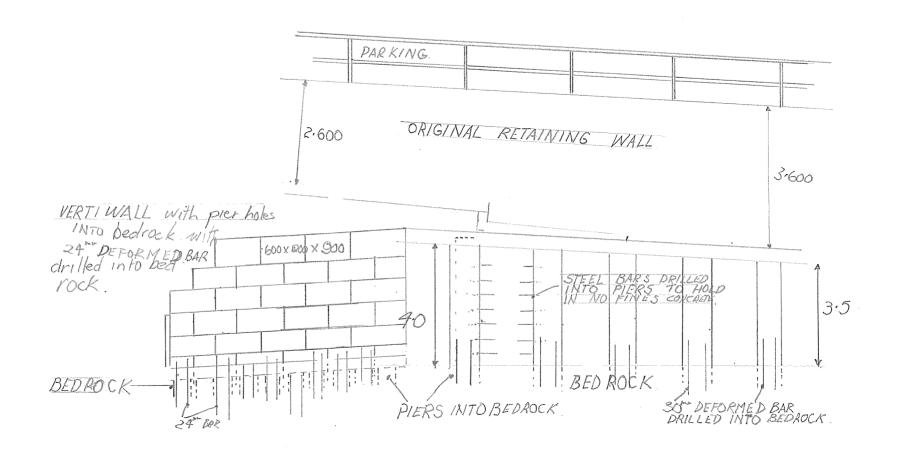




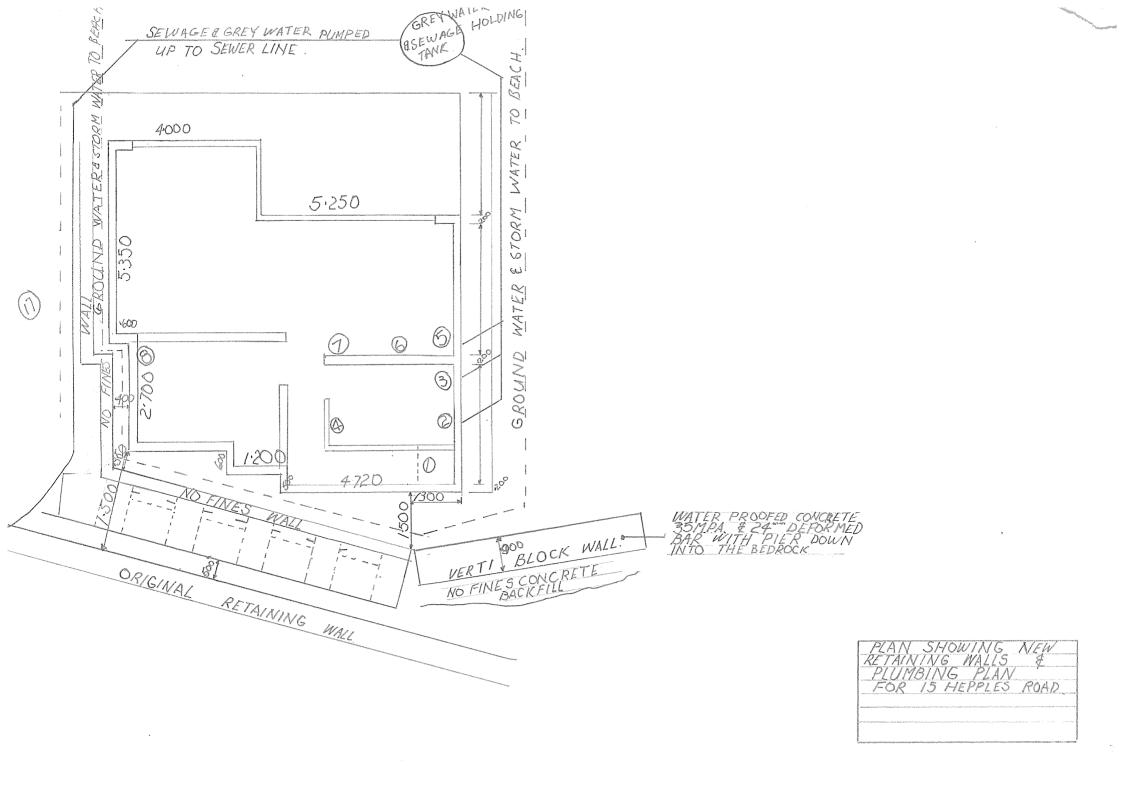


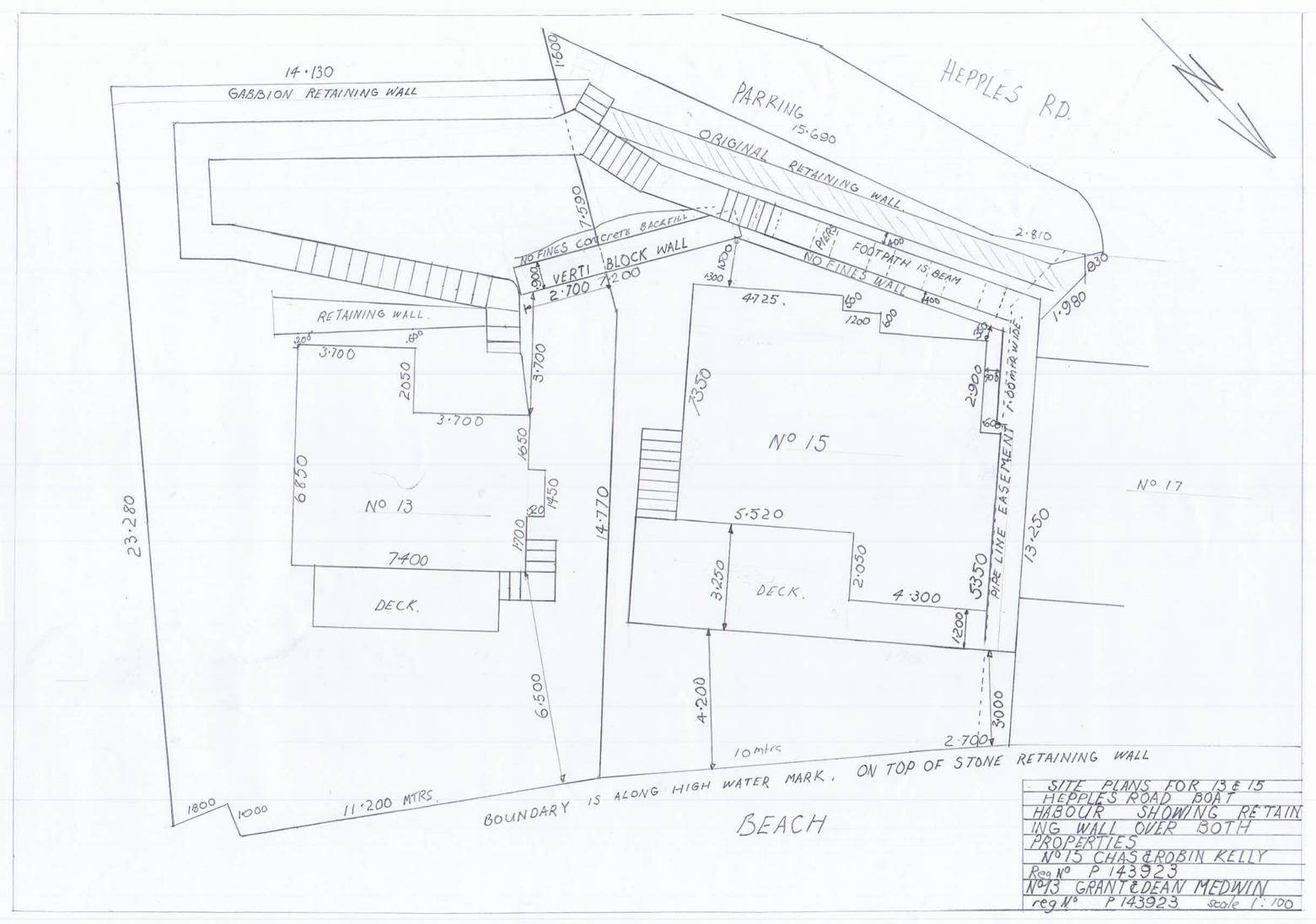
Appendix B

Development Plans



PLANS SHOWING NEW
RETAINING WALLS.





RENOVATED HOUSE FOR CHAS & ROBIN KELLY,
15 HEPPLES R.D. BOATHABOUR, 7321

LANDTITLE REF. P143923 131

DESIGN WIND SPEED IN 3

SOIL CLASSIFICATION CLASS

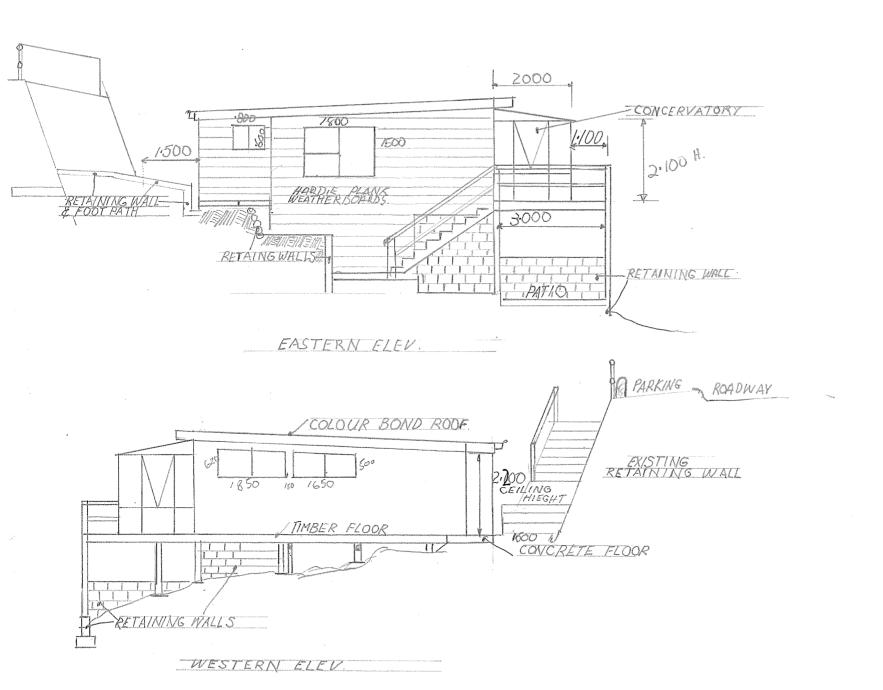
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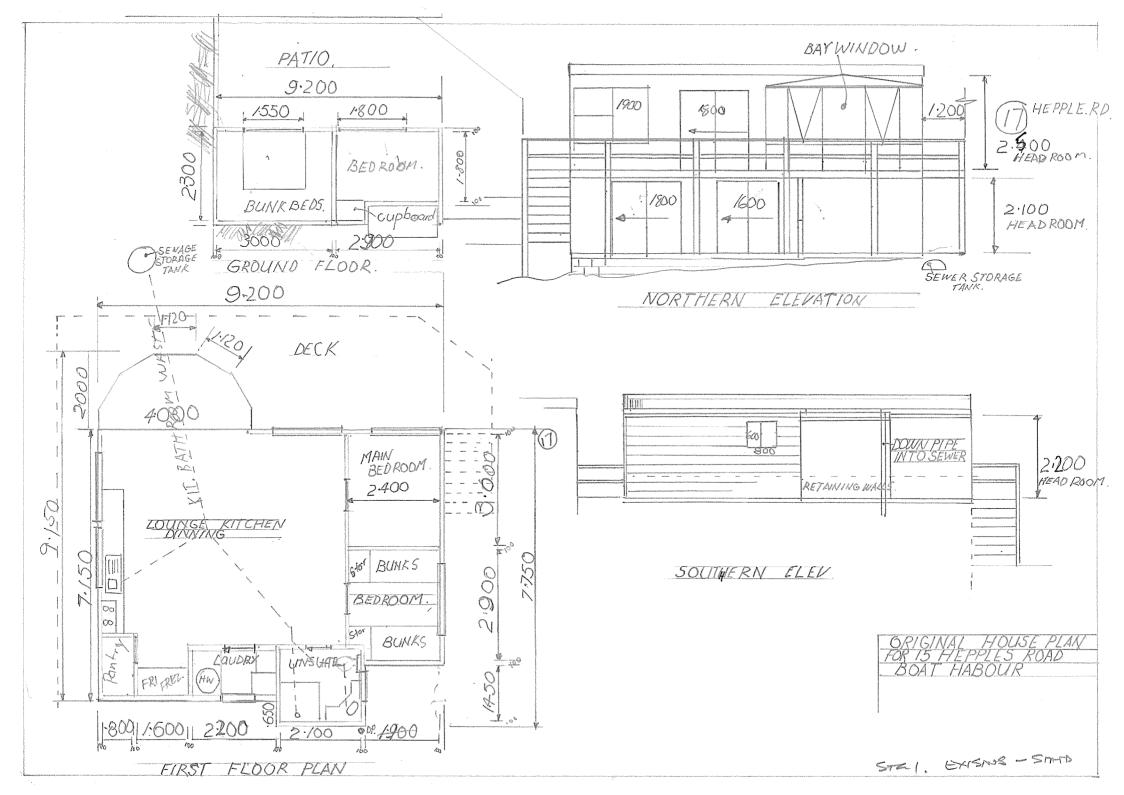
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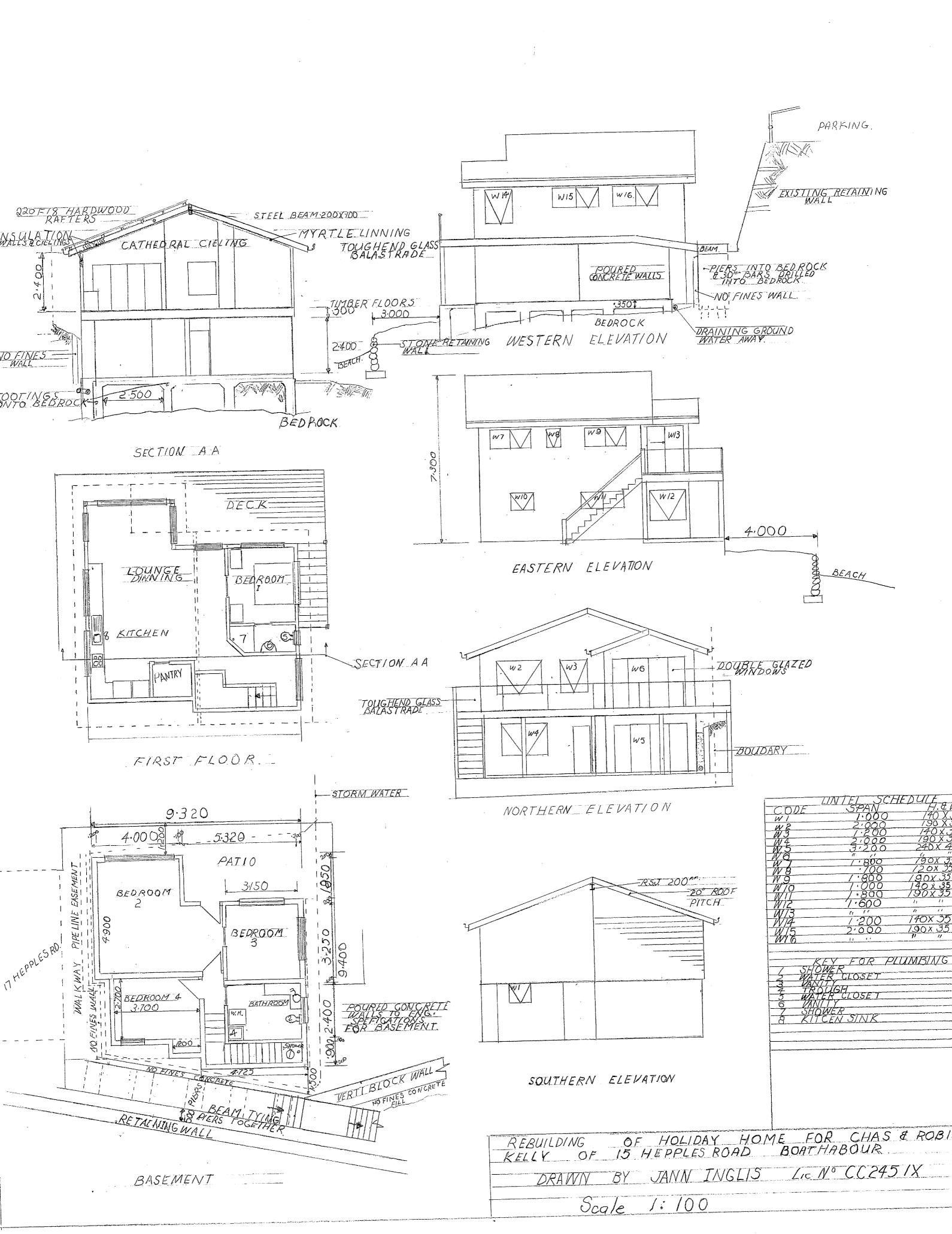
BUSHFIRE ATTACK LEVEL N/A

DRAWING INDEX
FLOOR PLANS & ELEVATIONS
SECTION
ROOF FRAMING PLAN
STORMWATER & DRAIN AGE.

DRAWN BY JANN	IN GL15
P.O.BOX 868 ULVERSTON	VE TAS 73/5
LICENCE Nº CC245/X	RENOVATED HOUSE FOR
phone 036425/867	CHAS & ROBIN KELLY
mobile 0400743873.	15 HEPPLES RD
dated 5-12-2017	BOAT HABOUR . TAS 7321
phone 036425/867 mobile 0400743873.	RENOVATED HOUSE FOR CHASE ROBIN KELLY







Project: PROPOSED RESIDENCE RE-BUILD

Measured form and function Gty

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> W 6ty.com.au E admin@6ty.com.au

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The Charles
287 Charles Street
Launceston Tasmania
P (03) 6332 3300

57 Best Street
Devonport Tasmania
P (03) 6424 7161

6ty Pty Ltd ABN 27 014 609 900

Architectural ABP No. CC4874f Structural / Civil ABP No. CC1633i

APPROVED COMPANY ISO 9001 Quality

QMS Certification Services

15 HEPPLES ROAD
BOAT HARBOUR 7321

For: CHAS & ROBIN KELLY

Project: 17.077

Drawings:

Cover Sheet

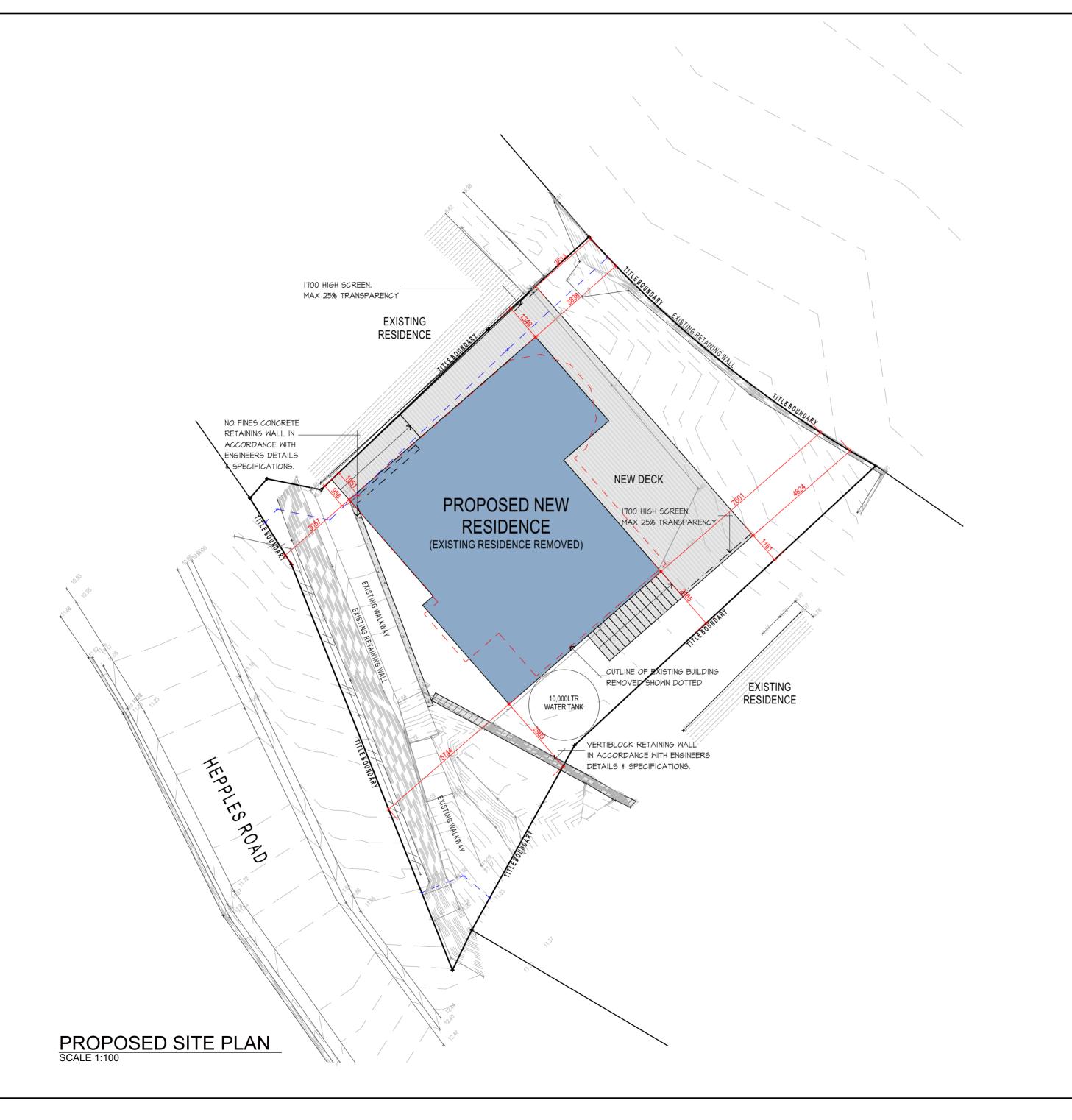
Ap01 SITE PLAN

Ap02 DEMOLITION, FLOOR & ROOF PLANS

Ap03 ELEVATIONS

DEVELOPMENT APPROVAL

Issue date: 17-09-2018



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Architectural ABP No. CC4874f Structural / Civil ABP No. CC1633i

APPROVED COMPANY

ISO 9001





PROJECT NORTH



PLANNING DOCUMENT

ISSUE	DATE	ISSUED FOR	REV.
01	17-09-18	DEVELOPMENT APPROVAL	-
02	17-01-19	DEVELOPMENT APPROVAL	-

DIMENSIONS ARE IN MILLIMETRES. DO NOT SCALE. CHECK AND VERIFY ALL DIMENSIONS ON SITE. REFER DISCREPANCIES TO THE SUPERINTENDENT. ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH: BUILDING CODE OF AUSTRALIA, APPLICABLE AUSTRALIAN STANDARDS & LOCAL AUTHORITY REQUIREMENTS.

PROPOSED RESIDENCE RE-BUILD

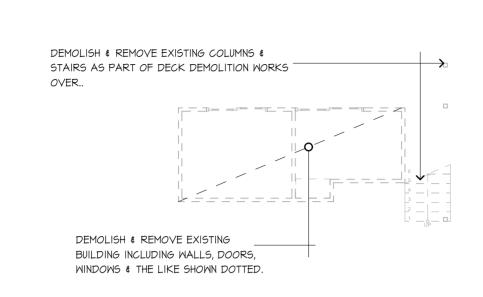
15 HEPPLES ROAD

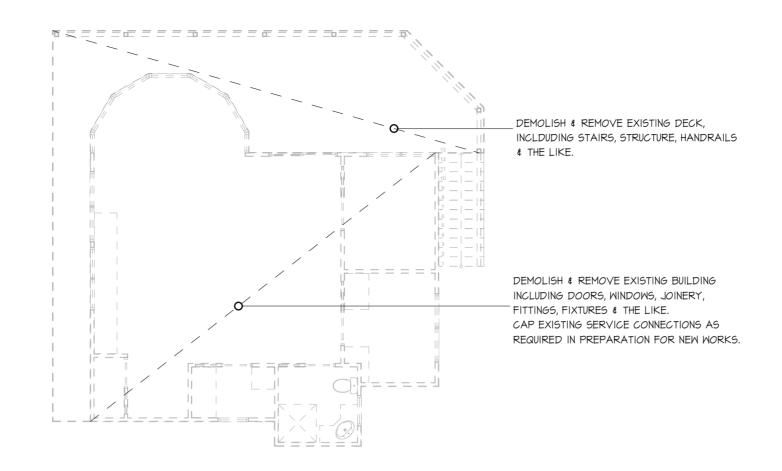
BOAT HARBOUR 7321 CHAS & ROBIN KELLY

DRAWING: SITE PLAN

PROJECT No. 17.077

DRAWING No. Apol Rev. -





6ty⁶

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Architectural ABP No. CC4874f Structural / Civil ABP No. CC1633i

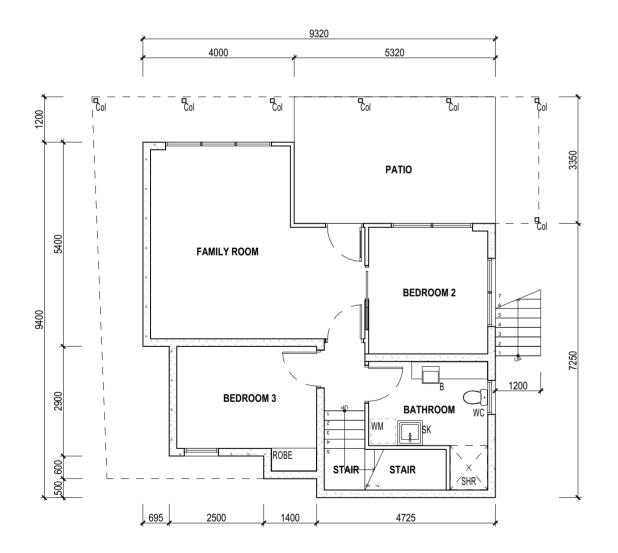
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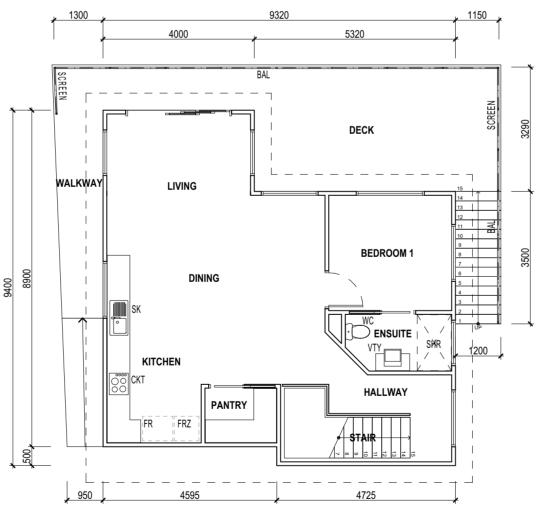
ISO 9001 Quality Nanagement Syste

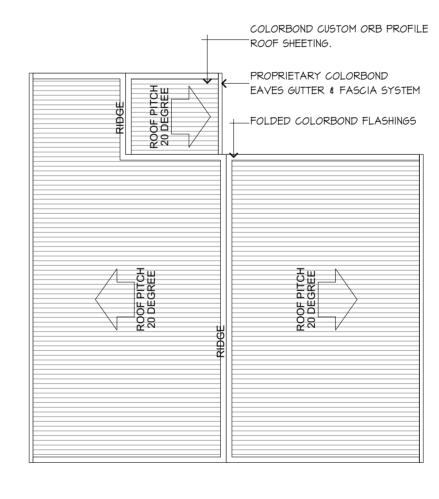
Management System

ONIS Certification
Services

PROPOSED GROUND FLOOR DEMOLITION PLAN SCALE 1:100 PROPOSED FIRST FLOOR DEMOLITION PLAN SCALE 1:100







PROPOSED FLOOR PLAN

PROPOSED FIRST FLOOR PLAN

PROPOSED ROOF PLAN
SCALE 1:100

PLANNING DOCUMENT

ISSUE	DATE	ISSUED FOR	REV.
01	17-09-18	DEVELOPMENT APPROVAL	-
02	17-01-19	DEVELOPMENT APPROVAL	-

DIMENSIONS ARE IN MILLIMETRES. DO NOT SCALE. CHECK AND VERIFY ALL DIMENSIONS ON SITE. REFER DISCREPANCIES TO THE SUPERINTENDENT. ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH: BUILDING CODE OF AUSTRALIA, APPLICABLE AUSTRALIAN STANDARDS & LOCAL AUTHORITY REQUIREMENTS.

PROPOSED RESIDENCE RE-BUILD

15 HEPPLES ROAD
BOAT HARBOUR 7321

FOR: CHAS & ROBIN KELLY

PLANS

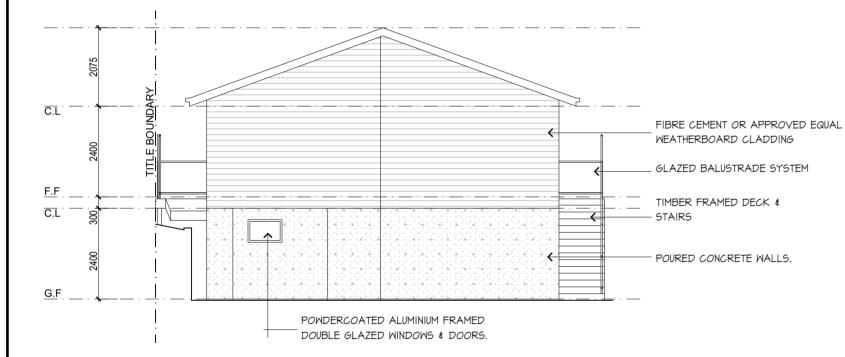
SIGNED: DVG DRAWN: ADB CHECKED: DVG

SCALES: 1:100 AT A2 SIZE DRAWING SHEET

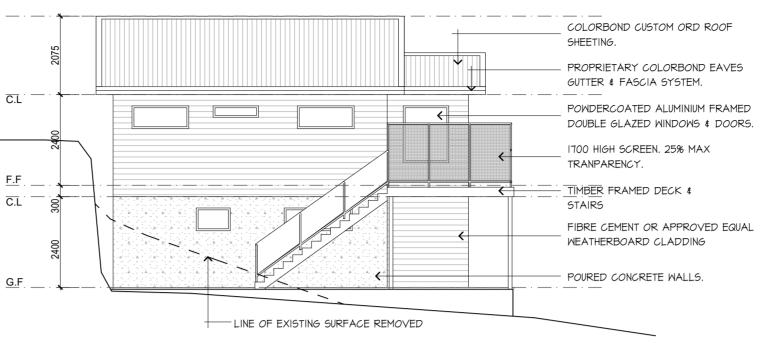
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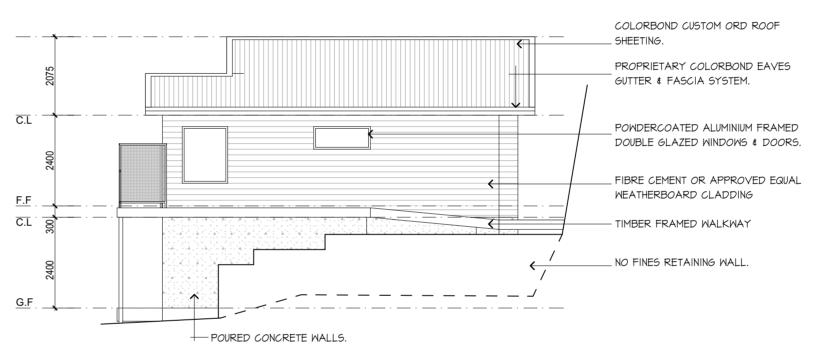
PROPOSED NORTH ELEVATION



PROPOSED SOUTH ELEVATION SCALE 1:100



PROPOSED EAST ELEVATION SCALE 1:100



PROPOSED WEST ELEVATION SCALE 1:100

Gty⁶

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ISO 9001 Quality Management Syster

QMS Certification Services

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PLANNING DOCUMENT

ISSUE	DATE	ISSUED FOR	REV.
01	17-09-18	DEVELOPMENT APPROVAL	-
02	17-01-19	DEVELOPMENT APPROVAL	-

DIMENSIONS ARE IN MILLIMETRES. DO NOT SCALE. CHECK AND VERIFY ALL DIMENSIONS ON SITE. REFER DISCREPANCIES TO THE SUPERINTENDENT. ALL WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH:
BUILDING CODE OF AUSTRALIA, APPLICABLE AUSTRALIAN STANDARDS & LOCAL AUTHORITY REQUIREMENTS.

PROPOSED RESIDENCE RE-BUILD

15 HEPPLES ROAD BOAT HARBOUR 7321

FOR: CHAS & ROBIN KELLY

DRAWING: ELEVATIONS

GNED: DVG DRAWN: ADR CHECKED:

SCALES: 1:100 AT A2 SIZE DRAWING SHEET

PROJECT No. 17.077 DRAWING No. Ap03 REV. -



Appendix C

Landslide Risk Assessment



LANDSLIDE RISK ASSESSMENT MODIFICATIONS TO DWELLING 15 HEPPLES ROAD, BOAT HARBOUR

Prepared for: **6ty**

Date: 9 April 2019

Document Reference: TG17185/1 - 02report Rev01

Tasman Geotechnics Pty Ltd ABN 96 130 022 589 16 Herbert Street, Invermay PO Box 4026, Invermay TAS 7248 T 6338 2398 E wayne@tasmangeotechnics.com.au

Document Set ID: 1042382 Version: 1, Version Date: 12/04/2019

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	2.4	Landslide Inventory	3	
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Important information about your report

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01

Document Set ID: 1042382 Version: 1, Version Date: 12/04/2019

Figures

Figure 1	Landslip A and B Zones at Boat Harbour
Figure 2	MRT Geology Map Extract
Figure 3	MRT Landslide Inventory Map Extract
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Appendices

Appendix A	Development Drawings
Appendix B	Landslip Survey Data
Appendix C	Rainfall Data
Appendix D	Selected Site Photographs
Appendix E	Engineering Borehole Logs
Appendix F	Laboratory Test Certificate
Appendix G	Landslide Risk Matrix
Appendix H	Risk to Life

Version	Date	Prepared by	Reviewed by	Distribution
Original	7 February 2019	Dr Alan Chester	Dr Wayne Griffioen	Electronic
Rev 01	9 April 2019	Dr Alan Chester	Dr Wayne Griffioen	Electronic

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01

1 INTRODUCTION

Tasman Geotechnics previously provided a Landslide Risk Assessment for the site at 15 Hepples Road, Boat Harbour title reference 143923/31 (report TG17185/1 – 01report, dated 23 March 2018).

The assessment was required as part of the Planning Application process, as the owner was issued an issues paper for:

- 1. Undertaking development without obtaining the necessary planning and building approvals; and
- 2. Building works being located within an A Landslip area.

However, no details of the proposed dwelling were available at the time.

On 7 June 2018, the Waratah-Wynyard Council requested additional information in relation to Development Application DA53/2018 for the demolition of an existing dwelling, replacement dwelling and retaining walls at 15 Hepples Road. The request for information noted that the Landslide Risk Assessment report "will need to take into consideration the demolition works, retaining walls, earthworks, and the proposed new dwelling…".

A set of drawings prepared by 6ty° was provided to Tasman Geotechnics as part of the current assessment: project 17.077, drawing Ap01, Ap02 and Ap03, dated 17 September 2018, as well as a drawing showing the pre-development survey and as-constructed bored piers under one of the retaining walls. The drawings are included in Appendix A of this report.

This revised report is a stand-alone document, and contains the information presented in our previous Landslide Risk Assessment.

Our scope of work consisted of:

- Reviewing maps and reports in the public domain (eg MRT website) and by direct discussions with MRT personnel;
- Carrying out a site walkover to note geomorphological features associated with landslide activity at the site, and of geological features in the larger Boat Harbour area;
- Drilling one borehole (BH1) using a track mounted drill rig to determine subsurface conditions at the site;
- Using results from our previous investigation on Hepples Road (with permission from Waratah-Wynyard Council).
- Performing a Landslide Risk Assessment.

The assessment is consistent with the Landslide Risk Assessment guidelines published by the Australian Geomechanics Society (2007).

2 BACKGROUND INFORMATION

2.1 Implications of Landslip A Zone

The extent of Landslip A and B zones at Boat Harbour is shown in Figure 1, and shows the existing site is wholly within Landslip A Zone.

It is our understanding that the provisions of the Building Act 2000 and Building Regulations 2014 remain applicable until the new Tasmanian Planning Scheme comes into effect.

For an A landslip area, the Tasmanian Building Act 2000 states that

- (1) A person must not erect, alter or add to a building in an A landslip area except in accordance with subsection (2)
- (2) The minister, on the recommendation of a general manager, may permit a person to -

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01

- (a) Erect, in an A landslip area-
 - (i) A shed; or
 - (j) An insubstantial building; or
- (b) Carry out building work, other than erections, in respect of a building in an A landslip area; or
- (c) Erect a building within the boundaries of a wharf in an A landslip area.

The Building Regulations stipulate that a person may only erect, alter or add to a building in a B landslip area if the total floor area will not exceed 200m² when the building work is completed. The Building Regulations also state that a permit may be issued for a building with more than 200m² floor area, if a certificate is given by a geotechnical engineer confirming that:

- i) the erection, alteration or addition can be carried out safely, and
- ii) the building will be structurally sound, and
- iii) the completed building will not affect the stability of the land.

In landslip areas, a person may only (Clause 13, Building Regulations 2014):

- a) Excavate or deposit, material in a landslip if the excavation or deposition is carried out in such a manner as to allow rainwater or seepage to drain from the site; or
- b) Permanently excavate or deposit any material for, or in connection with, building work in a landslip are if
 - i. The excavation is not more than 600 millimetres in depth; and
 - ii. The material, when deposited, is not more than one metre in height above ground level and is compacted and graded so as not to aggravate existing landslip conditions; or
- c) Backfill a trench or hole in a landslip area if the trench or hole is backfilled with well compacted material which was previously removed from the trench or hole; or
- d) Fell or remove trees or other vegetation for, or in connection with, building work on land in a landslip area if the person has obtained the written agreement of a permit authority; or
- e) Use any earth-moving or vibrating compaction equipment for, or in connection with, building work on land in a landslip area if the person has obtained the written agreement of a permit authority.

Thus, the works carried out to date have contravened a number of limitations relating to an A landslip area:

- Adding or altering a house
- Carrying out building work
- Permanently excavating more than 600mm of soil

2.2 Regional Setting

Boat Harbour is a seaside town built at the base of a steep coastal escarpment with a sheltered beach as the main attraction. Many of the houses were initially holiday shacks and still display their origins.

A prominent headland, Table Cape is situated to the east of the town and a rugged rocky coastline extends to the west. To the south a steep escarpment rises to a plateau approximately 120m above sea level.

The site is at the base of a steep escarpment facing north east and located at the edge of Boat Harbour Beach. At high tide water laps the front boundary of the property.

The township of Boat Harbour has been built over a complex of landslides and the site subject to this investigation is built at the toe of an active landslide.

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01

2.3 Geology

The Mineral Resources Tasmania (MRT) 1:25,000 Series Digital Geological map, Wynyard Sheet, shows the site to be mapped on Tertiary aged, weathered basalt. Quaternary aged landslide deposits are mapped immediately north of the site (17 Hepples Road).

An extract of the MRT geology map is presented on Figure 2.

2.4 Landslide Inventory

In 2010, MRT published the "Tasmanian Landslide Hazard Series" maps which includes 6 maps for the Wynyard area. Of particular interest is the Landslide Inventory map, which shows 7 landslides of different scale in the Boat Harbour township and another 5 along the access road (Port Road).

The site is located on an active landslide that is located on the toe of a larger (dormant) landslide that extends from the escarpment to the beach. For the purposes of this report this is referred to as the "Hepples Road Complex". A larger dormant complex is located 250m north of the site and this is termed as the "Town Complex". The 5 landslides along Port Road are referred to collectively as the "Port Road Slide". Two smaller, probably dormant, landslides are located on the escarpment between the "Hepples Road complex" and "Town complex", and these are referred to as "escarpment slides".

The Landslide Inventory Map also shows that there have been reports of damage to dwellings in the Boat Harbour township.

An extract of the MRT landslide inventory map is shown in Figure 3.

2.5 Geomorphology

A geomorphology map is included as part of the *"Tasmanian Landslide Hazard Series"* maps. The hill slope around Boat Harbour township has several distinct geomorphological features as shown in Figure 4.

- An abandoned coastal cliff (Ce), marked by a major convex break in slope
- Several midslope benches (Db)
- A narrow alluvial fan (Af)
- A narrow marine terrace at 15m above sea level (Cmt15) with a clearly defined terrace riser, and
- Beach.

There are no dunes in the bay. A number of landslides (identified in Section 2.4) have covered the original morphology.

The toe of the landslide is characterized by a convex break in slope, that is mapped immediately above the site.

2.6 Landslide Susceptibility Mapping

For the basalt soils of the North-West coast of Tasmania, MRT have identified two scales of landslides:

- Deep-seated rotational landslides: and
- Shallow slides or debris flows.

Landslide susceptibility maps for both scales of land sliding have been developed by MRT, and extracts are presented in Figure 5.

Susceptibility zones for first time deep-seated failures were developed by MRT by statistical analysis of slope geometry and geological material of known landslides, and are mapped as possible source, regression and runout areas associated with potential landslide movement. For the Tertiary basalts, threshold values of source, regression and runout areas are 14°, 20° and 16° respectively.

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For shallow slides and debris flows, the susceptibility for source area is also based on slope angle:

• High: greater than 20°

Moderate: between 10° and 20°

Low: between 6° and 10°

Very Low: less than 6°

The Wynyard Deep-seated Landslide Susceptibility Map shows that the site is located on a source area. The area is also mapped as Moderate to High susceptibility for shallow slides and debris flow.

2.7 Previous Investigations

Boat Harbour has had a history of landslides some of which have damaged buildings and others damaged roads and other infrastructure. A search of the MRT website identified 5 reports on landslides in the Boat Harbour Beach area. Three of these were considered relevant to the present investigation: Jennings (1965), Matthews (1972) and Matthews (1974). In addition, we obtained a copy of a Coffey Geosciences report (dated 2001), commissioned by DPIPWE and Waratah-Wynyard Council. We also used information from an investigation carried out by Tasman Geotechnics at Hepples Road for Waratah-Wynyard Council in 2016 (report TG16160/1 – 01report, dated 10 March 2017).

Jennings (1965) identified the risks for Port Road crossing a landslide and recommended that an alternative route be found to access the town. Jennings also stated that the use of septic tanks and careless disposal of drainage water was aggravating an already dangerous situation in relation to landslides.

Matthews (1972) explained that the risk of landslides in Boat Harbour area were due to deeply weathered basalt forming clays which when saturated were liable to move. Matthews mapped the Hepples Road Complex.

A comprehensive report on the landslide crossing Hepples Road by Matthews (1974) identifies some of the issues that characterize the area;

- Groundwater flow through the basalt talus appearing as springs above the basalt bedrock near the foreshore,
- Subsidence by 1m of a 128m long section of road, and
- Identification of a landslide extending about 230m uphill from the beach, that was active in 1969.

Coffey Geosciences (2001) undertook an investigation for the Department of Primary Industries Water and Environment and Waratah-Wynyard Council to provide a landslide risk assessment for the town. In this report Coffey Geosciences defined geomorphological units and described the existing landslides. The mapping produced by Coffey Geosciences is very similar to the landslide maps produced by MRT in 2010. The risk of loss of life for landslides was assessed to be very low. Coffey Geosciences also stated that movement on the landslide crossing Port Road was "Almost Certain" which has proved to be true.

The Tasman Geotechnics investigation in 2016 involved drilling 2 boreholes through Hepples Road with a truck mounted rig, using both hollow stem augers and diamond drilling (boreholes TGBH1 and TGBH2). Piezometers were installed in the boreholes to allow measurement of groundwater levels. One undisturbed soil sample (U63) was submitted to Chadwick Geotechnics to determine effective strength parameters by triaxial testing. Results of the 2016 investigation are included in the discussion in Section 4.

Waratah-Wynyard Council provided survey data gathered by PDA Surveyors of survey markers placed in the Hepples Road/Fenton Crescent area. The markers were placed and surveyed in 2004, and re-surveyed in 2009, 2016 and 2018. The data is presented in Appendix B and shows two markers on Hepples Road have moved around 400mm between 2009 and 2018, equivalent to approximately 45mm/yr.

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2.8 Rainfall

As rainfall is often a trigger for landslide movement, we obtained monthly rainfall records for Boat Harbour (opened in August 2012). The data for Boat Harbour is relatively recent, so we also obtained data for Mawbanna (opened since 1981). The data are presented in Appendix C.

Comparison of the monthly rainfall between 2012 and 2018 at the two stations shows is a strong linear correlation, with Mawbanna reporting up to 70% more rainfall than Boat Harbour. The typical ratio is 20%.

Similarly, the annual rainfall for Mawbanna is higher than Boat Harbour. Gaps in the monthly data mean that there are no pairs of years with complete rainfall data. Thus, the correlation for the annual rainfall is not as strong as the monthly rainfall data.

Nevertheless, the strong linear correlation for the monthly rainfall data means that the rainfall from Mawbanna can be used to interpret landslide movements at Boat Harbour.

The rainfall data shows that the driest month is February (46mm mean rainfall for Mawbanna) and the wettest month is July (177mm mean rainfall for Mawbanna). At Mawbanna there have been 3 occasions since records commenced in 1982 where the monthly rainfall has been more than 300mm ("significant rainfall"), and twice where it was marginally less than 300mm. Table 1 compares the corresponding rainfall at the two stations for these occasions.

 Month
 Mawbanna (mm)
 Boat Harbour (mm)

 July 1996
 292
 No data

 May 2007
 298
 No data

 August 2009
 331
 No data

 August 2013
 423
 356

Table 1. Monthly rainfall over 300mm for Mawbanna

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Figure B1 in Appendix B shows the movement at the survey markers along Hepples Road and the "significant rainfall" events. It is noteworthy that very little movement occurred between 2004 and 2009, despite a monthly rainfall close to 300mm at Mawbanna in May 2007. Therefore, the "significant rainfall" events in August 2009 and August 2013 more than likely caused in movement between 2009 and 2016. There is a definite increase in rate of movement after the July 2016 rainfall event.

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2.9 Proposed Development

July 2016

The original building at the site comprised a light weight structure, about 9m x 9m in plan. The floor level of the building was about 3m above the rock wall located along the beach. Due to the sloping nature of the site, two small rooms had been constructed under the main part of the building, creating the appearance of a 2 storey building. A survey of the original building is included in Appendix A and selected photographs of the original building are presented in Appendix D.

The new dwelling has a similar footprint as the original building, but is double-storey for the whole footprint. Thus, a significant volume of soil has been excavated: as much as 2m on the road-side of the house and along the boundary with 17 Hepples Road.

At the time of our fieldwork in September 2017, the ocean-side of the original dwelling was still present, while the road-side part had been reconstructed.

Two new retaining walls have been constructed at the road-side of the property; one from no-fines concrete and the second from pre-cast verti-blocks. Photographs supplied by 6ty° show a number of bored piers were installed below the no-fines concrete retaining wall. The piers are reportedly 3m deep. A drawing with the as-constructed piers is included in Appendix A.

In addition, a no-fines concrete retaining wall is located along the boundary with 17 Hepples Road.

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We do not know if subsoil drainage was installed behind the walls.

Floor and walls for a new development have been constructed from concrete and consist of two rooms. From the presence of plumbing fittings it would appear one room is intended to be a bathroom. The building is located about 0.3m away from the new retaining wall.

We understand no additional work has been carried out at the site since September 2017.

3 FIELD INVESTIGATION

The fieldwork was carried out by an Engineering Geologist from Tasman Geotechnics on 21 September 2017. The fieldwork involved the following:

- Inspection of the site to determine the extent of works carried out,
- Inspection of the surroundings to note features relevant to landslip in the area around the site,
- Taking photographs of the site, and
- Drilling one borehole (BH1) to 5m below ground level using a track mounted rig to determine sub-surface conditions below the site. Due to the limited area on the site it was not possible to drill more than one borehole.

Selected photographs are presented in Appendix D. The borehole log for BH1 as well as the borehole logs for the Hepples Road investigation (TGBH1 and TGBH2) are presented in Appendix E, together with a photographs of the core. Surface features relevant to this investigation and locations of current and previous boreholes by Tasman Geotechnics are shown on Figure 6.

No soil samples were taken during the investigation as the sub-surface soil was a mixture of rock fragments and soil, unsuitable for testing. Nevertheless, some laboratory testing was reported by Tasman Geotechnics from the investigation at Hepples Road. The results of the laboratory testing are discussed in Section 4.3.

4 RESULTS

4.1 Surface Conditions

Most of the observations described here are shown in Figure 6.

Substantial works have been done on the site so very little natural topography is present. The only piece of natural topography may be the small grassed area that extends from the front of the existing dwelling to the beach. However a rock retaining wall has been built along the beach boundary so much of this ground could be fill.

The borehole was located on the eastern side of the dwelling on ground which appears to have been excavated approximately 1.5m below the natural topography. This estimate is based on the level of apparently natural ground beneath the existing original dwelling. This excavation was probably carried out at the time the original shack was constructed.

The south western boundary of the property adjoins Hepples Road. A no-fines concrete retaining wall has recently been constructed along half of this boundary. This wall is approximately 3m high. It would appear to be founded on talus. Photographs provided by 6ty° indicate bored piers were installed below the retaining wall and joined with a ground beam. The piers are reportedly 3m deep. The wall was constructed in front of a 5m high crib wall. The crib wall continues above the concrete wall, and was originally constructed to support Hepples Road.

A verti-block wall has recently been constructed along the other half of the south western boundary. No foundation or drainage details are known for the wall.

On the uphill side of Hepples Road there is a block retaining wall. The grassed areas uphill of this wall have a hummocky appearance indicative of landslip.

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Houses adjacent to 15 Hepples Road (to each side and uphill) have been damaged by landslide movement as indicated by buckled walls, leaning columns supporting verandahs, misaligning doors and windows. A photograph of 15 Hepples Road before the current reconstruction works also shows gaps in the external walls.

The following observations were made of the slopes uphill of the site:

- The surface of Hepples Road and concrete kerbing has cracks and undulations indicative
 of ground movement.
- Tension cracks were observed in the grass at 2 and 10 Hepples Road in 2016.
- Port Road, immediately uphill of 1 Fenton Crescent, has a small step (<100mm high) that was repaired in 2018.
- Large basalt boulders are present on the vacant lot adjacent to 237 Port Road.
- The head scarp of the Hepples Road Complex is located near an outcrop of basalt rock, about 200m inland and at 70m above sea level. A backward rotated block forms an area of internal drainage that collects surface runoff.

4.2 Subsurface Conditions

Excavations under the existing dwelling show a profile of talus for the exposed 2.0m on the western side. On the eastern side a talus profile of at least 1.5m is exposed.

BH1 was advanced to 1.3m using auger drilling, where the auger refused on boulders. The borehole was continued using diamond drilling (HQ coring) to a final depth of 5m below the current ground level.

The subsurface profile at BH1 comprised:

- Talus (clay with occasional cobbles) to 1.3m below current ground level, overlying
- Boulders and cobbles within a silty clay matrix to 2.7m below current ground level, overlying
- Fractured basalt bedrock, black, high strength to at least 5m below ground level.

The subsurface conditions under Hepples Road, based on the investigation by Tasman Geotechnics in 2016 (TGBH1 and TGBH2), are as follows:

- FILL, comprising layers of road base, gravelly sand, and clayey sand, to 1.6m below road level, overlying
- TALUS: SILTY CLAY, high plasticity, red/brown, with basalt boulders and cobbles to 3.5m below road level in TGBH1 and 5.7m below road level in TGBH2, overlying
- RESIDUAL SOIL, presenting as gravelly clay, high plasticity, brown, to 4.6m in TGBH1 and 6.8m in TGBH2, overlying
- BASALT BEDROCK, fine grained, black/blue, highly to distinctly weathered, medium rock strength, fractured. The highly weathered basalt has very low rock strength, while the distinctly weathered basalt has medium rock strength.

The basalt bedrock encountered in the present investigation was similar to that encountered in the 2016 investigations.

While standpipe piezometers were installed in TGBH1 and TGBH2, no groundwater was measured in them (dry to 5.5m below road level). Photographs supplied by 6ty show there was water in the bottom of the bored piers after they were excavated. Due to the drilling method used for the present investigation (diamond drilling), no groundwater level could be measured in BH1.

Based on photographs provided by 6ty°, we understand that bored piers were installed below the no-fines concrete retaining wall to 3m below the footing level. From our borehole profile, we expect this is at the top of the basalt bedrock. Therefore, the piers are not embedded in the rock.

Talus is resting on steeply sloping bedrock consisting of basalt in turn overlying quartzite. As ground water is seeping out at beach level over the top of basalt bedrock we assume the talus is

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sliding on the bedrock, particularly when the groundwater level is elevated, as is the case after high rainfall events.

A schematic cross section from the beach to Hepples Road is presented in Figure 7.

4.3 Soil Properties

While no laboratory testing was carried out for the present investigation, laboratory results were reported by Tasman Geotechnics for the investigation of Hepples Road:

- Atterberg Limits and field moisture content testing was carried out by Tasman Geotechnics.
 Although not a NATA accredited laboratory, the testing was carried out in accordance with Australian Standard methods.
- Triaxial testing (consolidated undrained with pore pressure measurement, CUPP) was carried out by Chadwick Geotechnics, a NATA accredited laboratory in Victoria. The laboratory certificate is presented in Appendix F.

Laboratory results for the Atterberg Limits are presented in Table 2.

Table 2. Laboratory Test Results

Material	Clay	Clay (residual soil)
Depth (m)	TGBH2: 2.0-2.2	TGBH1: 3.1-3.3
Liquid Limit (%)	66	77
Plastic Limit (%)	33	33
Plasticity Index (%)	33	44
Linear Shrinkage (%)	16	18

Thus, the natural clay is high plasticity clay (Unified Soil Classification Symbol CH).

The field moisture content of various samples are summarized in Table 3.

Table 3. Soil Moisture Contents

Depth (m below road level)	TGBH1	TGBH2
2 to 2.2	-	55
3.1 to 3.2	57	64
3.9 to 4.1	49	59
5.5 to 5.6	-	36

Thus, the field moisture contents are generally above 50% and approaching the Liquid Limit shown in Table 2. In TGBH2, the moisture content at 5.5m depth is close to the Plastic Limit. However, this is interpreted to reflect the gravelly nature of the soil.

The triaxial test was carried out on a sample from TGBH1 at 2.45m to 2.95m depth. The test provides effective strength parameters, ϕ ' and c', that are typically used to analyse the long-term stability of slopes. The sample tested for this investigation showed ϕ ' = 27°, and c' = 0kPa. As the sample is of the talus, it is likely to have been subject to previous landslide movement. Therefore, the strength parameters probably represent "remoulded" conditions.

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5 GEOTECHNICAL MODEL

5.1 Geological History

To understand why landslides are a particular problem in Boat Harbour it is necessary to understand the geological history of the site and its surrounds. A brief summary of the geological history of Boat Harbour area follows.

The basement rocks, now quartzite, were deposited as sandy sediments on the floor of a shallow sea during Mesoproterozoic times. Ripple marks still evident in some beds can be used to determine depositional depths below wave base. Age determinations have been based on radiometric dating of detrital zircons. Later sedimentation included siltstone and dolomite sequences which can now be seen west of Boat Harbour.

Orogenic movements caused folding and faulting at intervals, early Neoproterozoic to Cryogenian and again Ediacaran to Cambrian. A major fault known as the Boat Harbour Fault, prominent between Boat Harbour and Sister's Beach, probably occurred during the Wickham Orogeny at approximately 760Ma.

Unconformities are present at a number of levels indicating periods of erosion.

Major folding occurred due to a terrane collision during the Cambrian. The terrane boundary is marked by the Arthur Lineament which runs from the north coast just east of Boat Harbour to Ahrberg Bay on the west coast. Rocks within the lineament are intensely folded and high pressure metamorphic affects are prominent.

Further deposition and erosion occurred after the Cambrian but the next major event of significance to landslide activity was the opening of Bass Strait. This subjected the underlying quartzite to further erosion and wave cut activity at times. The sea levels rose and fell so that wave cut platforms developed at a number of levels. Steep slopes formed on the tilted quartzite beds and sharp ridges formed due to the hard rock.

Volcanic activity occurred at approximately 13Ma (basalt date from Tollymore Road, just south of Boat Harbour) and Table Cape was a major volcanic centre which poured basalt lava across the pre-Tertiary landscape. Lava flowed towards and past Boat Harbour and flowed down over the steep faces of the underlying rock forming the basement of what is now an escarpment.

In the time since the volcanic activity ceased the basalt has weathered into deep clays. The clay surrounding Boat Harbour is resting on steep flat surfaces offering very little frictional resistance to sliding so that when the clay becomes saturated it generates landslides.

Earthquake activity continues to occur on the northwest coast. A search of the GeoScience Australia database returned 9 earthquake events that occurred between 2002 and 2016 and were located between Devonport and King Island, with magnitudes ranging from 2.1 to 4.5. The 4.5 event occurred in February 2002 near King Island, and was felt at Burnie, Smithton and Strahan. Two events (magnitude 2.5 and 3.4) occurred northeast of Wynyard in January 2013.

5.2 Landslide Morphology

A number of landslides have been mapped close to the study site as indicated in Section 2.4. The Hepples Road Complex, located immediately north of 15 Hepples Road is directly relevant to the site. The landslide is known to have been active in 1969 (Matthews, 1974).

The head scarp for the Hepples Road Complex is mapped about 200m south west of the site, near the crest of the plateau. A backward rotated block forms an area of internal drainage that collects surface runoff and likely causes elevated groundwater levels within the landslide.

At Hepples Road the landslide exhibits creep, approximately 45mm/year. A number of houses, as well as Hepples Road and Port Road are affected by the creep. The house damage includes lateral movement and rotation of footings which in turn leads to gaps or jamming of windows and doors. Walls have buckled and retaining walls have started to lean and in some cases have broken. Hepples Road has developed tension cracks and small scarps. Tension cracks were observed in the grass at 2 and 10 Hepples Road. There is a small bump in Port Road where the landslide crosses it.

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The head scarp has a typical slope of 31°, while the main body has a slope of about 24°. The toe (from Port Road to the beach) has an average slope of 13°. A cross section of the Hepples Road complex is shown in Figure 8.

Port Road appears to mark the boundary between the zone of depletion (on the uphill side) and the zone of accumulation (on the downhill side). The landslide is about 70m wide. Based on borehole drilling, the zone of rupture is about 5m to 7m below ground level. The landslide volume is estimated to be about 100,000m³.

The landslide toe is located at the high water mark. Three boreholes at the landslide toe have confirmed basalt bedrock. Basalt rock outcrop also occurs at beach level. It is postulated that the basalt bedrock is steeply dipping from the rock outcrop near the head scarp to the beach.

Low retaining walls (less than 1m high) have been constructed along the shore line, and the high water mark is at these walls. Thus, the soils in the landslide toe can become saturated. Nevertheless, the base of the slide is not subject to erosion activity.

Two substantial retaining walls (greater than 3m high) have been constructed along the south western boundary of 15 Hepples Road. One of these, a no-fines concrete wall, has 3m long bored piers. However, the piers are not founded <u>in</u> the basalt bedrock, merely <u>on</u> the rock. No construction details are available for the other, a verti-block wall.

It appears that groundwater flows through the clay overlying the bedrock, and forms springs at beach level immediately above the rock surface.

The response of groundwater levels to rainfall has not been investigated or established. Nevertheless, monthly rainfall data since 1982 from the weather station at Mawbanna shows that "significant rainfall" events (ie more than 300mm per month) occurred in August 2009, August 2013 and July 2016, and that the survey markers installed since 2004 started moving after the August 2009 rainfall event.

6 LANDSLIDE RISK ASSESSMENT

6.1 General

Risk assessment and management principles applied to slopes can be interpreted as answering the following questions;

- What might happen? (HAZARD IDENTIFICATION).
- How likely is it? (LIKELIHOOD).
- What damage or injury might result? (CONSEQUENCE).
- How important is it? (RISK EVALUATION).
- What can be done about it? (RISK TREATMENT).

The risk is a combination of the likelihood and the consequences for the hazard in question. Thus both likelihood and consequences are taken into account when evaluating a risk and deciding whether treatment is required.

The qualitative likelihood, consequence and risk terms used in this report for risk to property are given in Appendix G and are based on the Landslide Risk Management Guidelines, published by Australian Geomechanics Society (AGS, 2007). The risk terms are defined by a matrix that brings together different combinations of likelihood and consequence. Risk matrices help to communicate the results of risk assessment, rank risks, set priorities and develop transparent approaches to decision making.

6.2 Potential Hazards

Based on the site observations, borehole data and available information discussed in the sections above, the following landslide hazards are identified for the site. Figure 9 illustrates the landslide hazards.

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Deep-seated "Hepples Road" landslide. This landslide extends 200m from the beach to the crest of the plateau. The main body of the landslide appears to be relatively stable, with movement confined to the toe. The rate of movement is assessed to be slow. However, the likelihood of movement for the main body of the landslide is assessed to be "Likely".

Movement of existing active landslide. Based on the historical information and MRT mapping, the new dwelling is located near the toe of an active landslide. We infer that the failure mechanism of the slide is due to talus sliding on the steep slope of underlying bedrock when lubricated by high groundwater levels. While there is no erosion at the toe of the slide, the soils are periodically wetted by high tides, resulting in softening of the soils. Seismic activity could also trigger landslide events, and recent minor earthquakes have occurred in the area. High rainfall events resulting in elevated groundwater levels at a regional scale almost certainly instigated the landslide movements. Impeded groundwater drainage or increased surface infiltration possibly combined with extensive excavation/erosion at the toe could lead to rapid movement. The rate of movement is currently about 45mm/year. The likelihood of movement of the existing landslide is assessed to be Almost Certain.

Small scale landslides (up to about 3m deep). Such landslides can occur where slopes are locally steep, or have been steepened by earthworks (cut or fill) and would involve up to 1,000 m³ of soil. Small scale landslides may also occur due to localized soil erosion (eg from poor control of surface runoff) and locally elevated groundwater levels (eg, seepage water collected in fill embankment).

Groundwater levels at the site are close to the surface at the beach, and approximately 2m below the floor level of the new construction.

The new construction is located in a cut which is about 2m below the original ground surface, this cut being within talus material. A no-fines concrete wall has been constructed along the steep slope below Hepples Road. While bored piers have been installed below the strip footing, the piers are not embedded in the basalt bedrock and have minimal reinforcement. The piers are not designed to resist shear forces or bending moments, and therefore do not provide resistance to sliding over the bedrock. Nevertheless, a crib wall is located immediately upslope of the no-fines concrete

The likelihood of a small scale slide in the slope between the road and house is assessed to be Unlikely, given the substantial retaining wall recently constructed. However, a small scale landslide may extend from Hepples Road below the bored piers. The likelihood of such a landslide is assessed to be Possible.

The identification of the potential hazards considers both the site and nearby properties, and is necessary to address stability issues that may negatively impact upon the site and influence the risk to property.

6.3 Risk to Property

The following table summarizes the risk to property of the landslide events in relation to the predemolition dwelling and the current development as described in Section 2.9.

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Table 4. Landslide risk profiles

Scenario		Likelihood	Consequence	Risk Profile	
Deep-seated landslide	previous dwelling	Likely	Medium: moderate damage to a number of properties	Very High	
	new dwelling and retaining walls	Likely	Medium: moderate damage to a number of properties	Very High	
Movement of existing active landslide	previous dwelling	Almost Certain during/after high rainfall events	Medium: moderate damage to a number of properties over a period of time	Very High	
	new dwelling and retaining walls	Almost Certain during/after high rainfall events	Medium: moderate damage to a number of properties over a period of time	Very High	
Medium scale slide in road embankment	previous dwelling	Possible	Major: extensive damage to house and road	High	
	new dwelling and retaining walls	Unlikely	Minor: while concrete walls will limit damage to the house, the road will require reconstruction	Low	
Medium scale rotational	previous dwelling	Possible	Major: extensive damage to house and road	High	
landslide from road under house	new dwelling and retaining walls	Possible for failure of road under bored piers.	Major: extensive damage to house and road	High	

The above assessment shows that the risk profile for the property with the previous dwelling was Very High to High. The risk profile for the property with the new dwelling and retaining walls is Very High to Low.

The Waratah-Wynyard Planning Scheme stipulates (Clause E6.6.2) that:

"If the site is within an area of risk shown on a natural hazard map...

- (a) a hazard risk assessment must determine -
 - (i) there is an insufficient increase in risk to warrant any specific hazard reduction or protection measure; or
 - (ii) a tolerable level of risk can be achieved for the type, form, scale and duration of the development..."

The risk assessment shows that there is no increase in risk profile for the individual landslides at the property given the new retaining wall and dwelling. At the same time, we note that owners of existing houses at Boat Harbour are generally aware of landslide issues. Therefore, no specific hazard reduction or protection measures are required. Thus, the requirements of Clause E6.6.2 are satisfied.

6.4 Risk to Life

The calculation of risk to life requires a quantitative assessment. Here, we have used an event tree approach to assess the risk to life for the person most at risk, a resident at the house.

Two event trees showing a possible sequence of events is presented in Appendix H for i) a medium scale landslide causing collapse of the road-side retaining wall, and ii) the deep-seated landslide causing distortion and collapse/failure of the house. The risk assessment shows that the Risk to

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Life for such those landslides and assuming management measures are incorporated in the design and construction of the house, is 9.7 x 10⁻⁵/annum.

AGS (2007c) suggests the tolerable loss of life for individual most at risk should be 10^{-5} /annum for new constructed slopes or new development, and 10^{-4} /annum for existing slopes. Thus, the calculated risk to life is marginally lower than the tolerable loss of life for an existing slope.

7 CONCLUSIONS

The landslide risk assessment presented here has shown that there are three landslides that could impact the site:

- The large scale active landslide
- · A medium scale landslide in the road embankment
- A medium scale landslide of the road and under the bored piers

The risk profile for the property with the new dwelling and retaining walls is Very High to Low.

The risk assessment has shown that there is no increase in risk profile for the individual landslides at the property given the new retaining wall and dwelling. Therefore the requirements of Clause E6.6.2 are satisfied.

The risk to life for individual most at risk is shown to be 9.7×10^{-5} /annum, where AGS (2007c) suggests the tolerable loss of life for individual risk should be 10^{-5} /annum for a new development or 10^{-4} /annum for an existing slope.

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Important information about your report

These notes are provided to help you understand the limitations of your report.

Project Scope

Your report has been developed on the basis of your unique project specific requirements as understood by Tasman Geotechnics at the time, and applies only to the site investigated. Tasman Geotechnics should be consulted if there are subsequent changes to the proposed project, to assess how the changes impact on the report's recommendations.

Subsurface Conditions

Subsurface conditions are created by natural processes and the activity of man.

A site assessment identifies subsurface conditions at discrete locations. Actual conditions at other locations may differ from those inferred to exist, because no professional, no matter how qualified, can reveal what is hidden by earth, rock and time.

Nothing can be done to change the conditions that exist, but steps can be taken to reduce the impact of unexpected conditions. For this reason, the services of Tasman Geotechnics should be retained throughout the project, to identify variable conditions, conduct additional investigation or tests if required and recommend solutions to problems encountered on site.

Advice and Recommendations

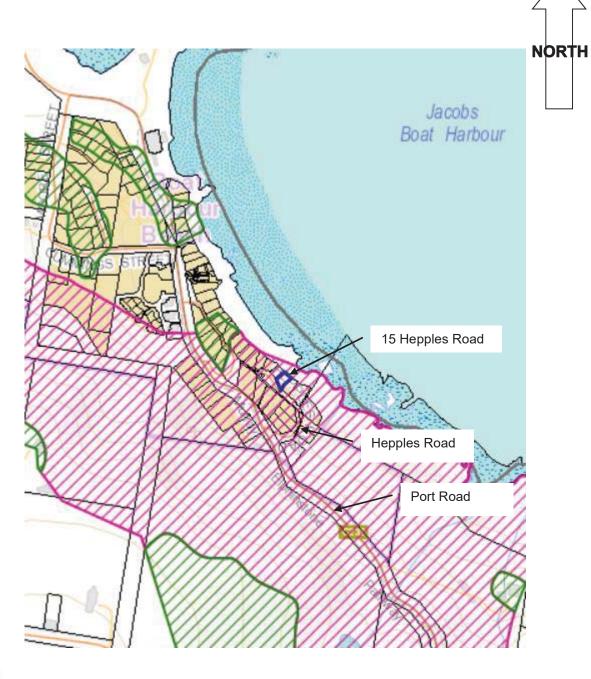
Your report contains advice or recommendations which are based on observations, measurements, calculations and professional interpretation, all of which have a level of uncertainty attached.

The recommendations are based on the assumption that subsurface conditions encountered at the discrete locations are indicative of an area. This can not be substantiated until implementation of the project has commenced. Tasman Geotechnics is familiar with the background information and should be consulted to assess whether or not the report's recommendations are valid, or whether changes should be considered.

The report as a whole presents the findings of the site assessment, and the report should not be copied in part or altered in any way.

TASMAN GEOTECHNICS

Rev 02, July 2018



☑ Zone A ☑ Zone B

drawn	WG
approved	WG
date	6/2/2019
scale	NTS
original size	A4

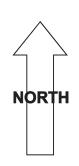
Version: 1, Version Date: 12/04/2019

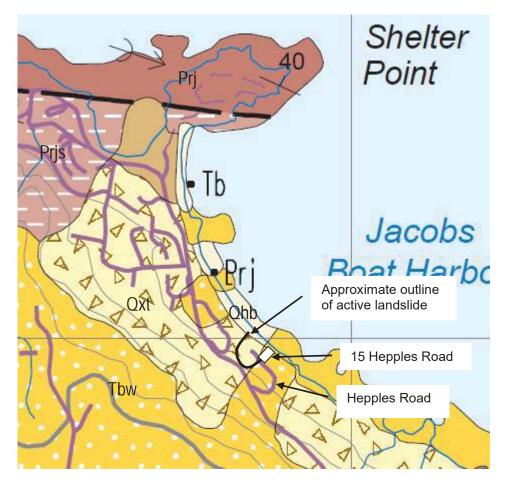


client:	6ty°
project:	Landslide Risk Assessment 15 Hepples Road, Boat Harbour
title:	Landslip A and B Zones at Boat Harbour

original size A4 geotechnics project no: TG17185/1 – 02report figure no: FIGURE 1

Document Set ID: 1042382



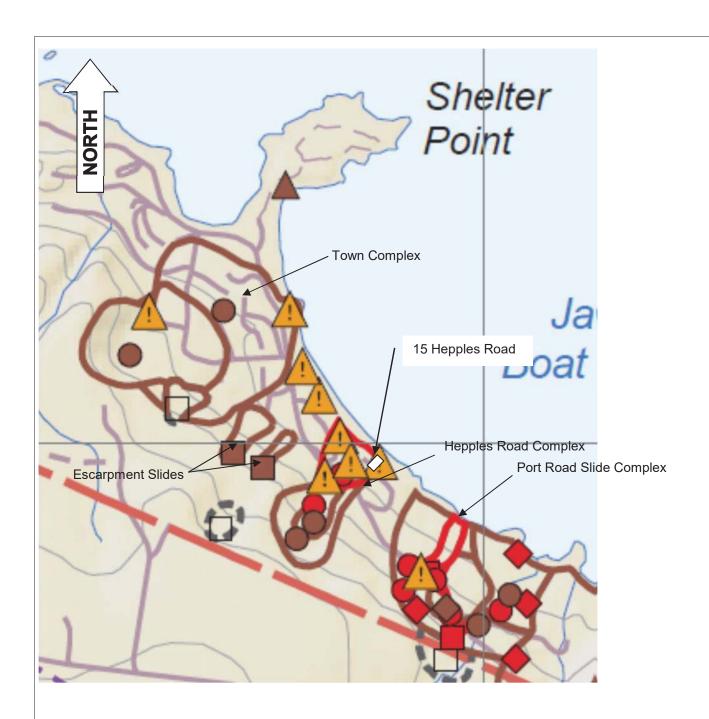


Beach sand (Qhb). Qhb Landslide deposits predominantly derived from weathered Tertiary rocks (Qxt). Qxt Predominantly deeply-weathered basalt (Tbw). Tbw Prjs Interbedded shaly black siltstone and thinly bedded quartzite (Prjs). Well-bedded, cross-bedded, mostly medium to coarse-grained orthoguartzite (Prj). (Jacob Quartzite). Prj

drawn	WG		client:	6ty°	
approved	WG	((3),	project:	Landslide Risk A	Assessment
date	4/12/2017		project.	15 Hepples Road,	Boat Harbour
scale	NTS	TASMAN	title:	MRT Geological	Map Extract
original size	A4	geotechnics	project no:	TG17185/1 – 02report	figure no: FIGURE 2

Document Set ID: 1042382

Version: 1, Version Date: 12/04/2019



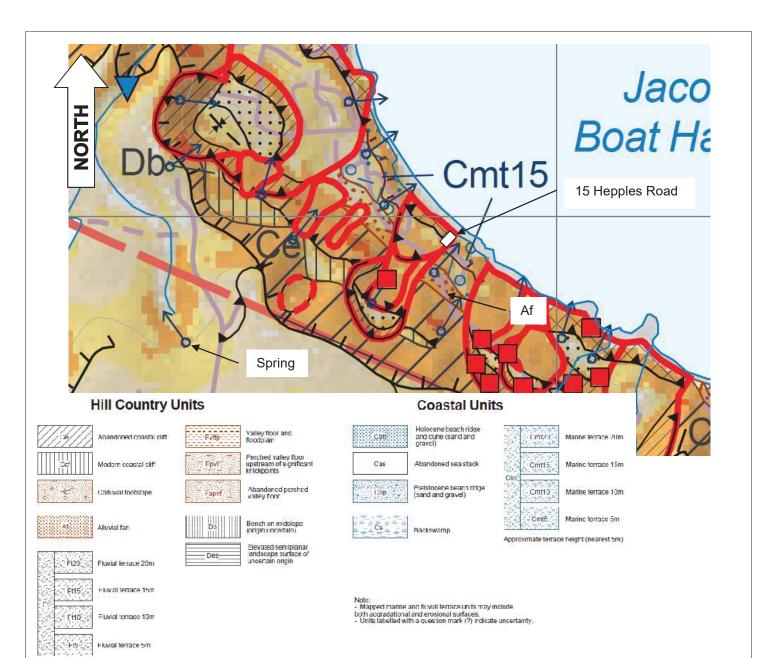
drawn	WG
approved	WG
date	4/12/2017
scale	NTS
original size	A4



client:	6ty°
project:	Landslide Risk Assessment 15 Hepples Road, Boat Harbour
title:	MRT Landslide Inventory Map Extract

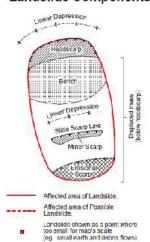
project no: TG17185/1 - 02report

figure no: FIGURE 3



Approximate terrace height (nearest 5m)

Landslide Components

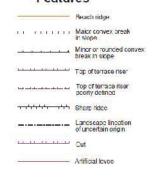


Slope Categories



Note: The techniques used to create the slope layer tend to underestimate values along cliffs

Linear Geomorphic Features



drawn	WG	
approved	WG	
date	21/1/2019	
scale	NTS	
original size	A4	

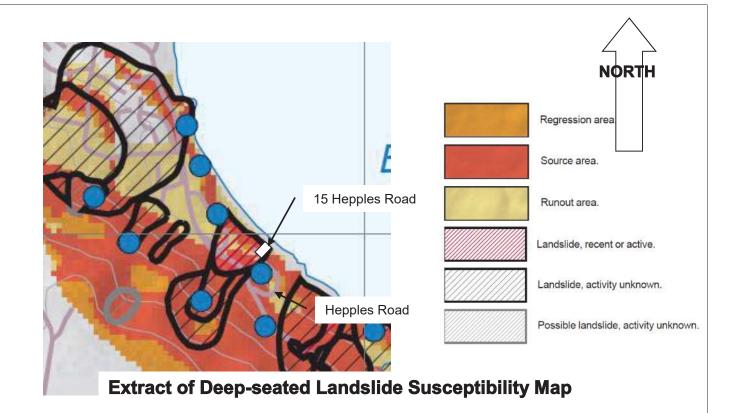
TASMAN geotechnics

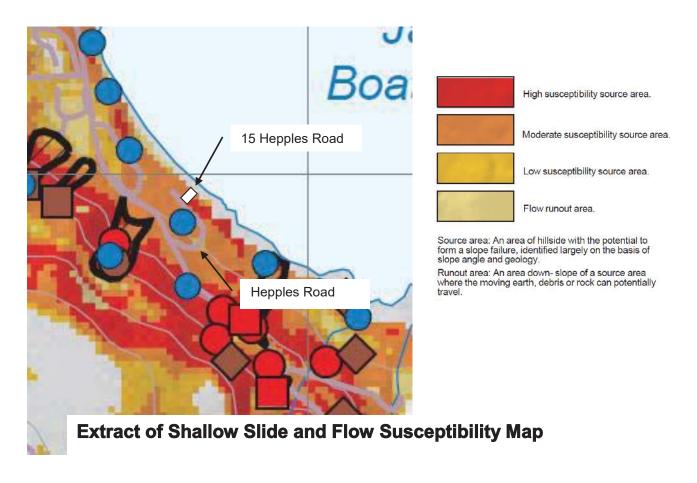
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project: Landslide Risk Assessment
15 Hepples Road, Boat Harbour

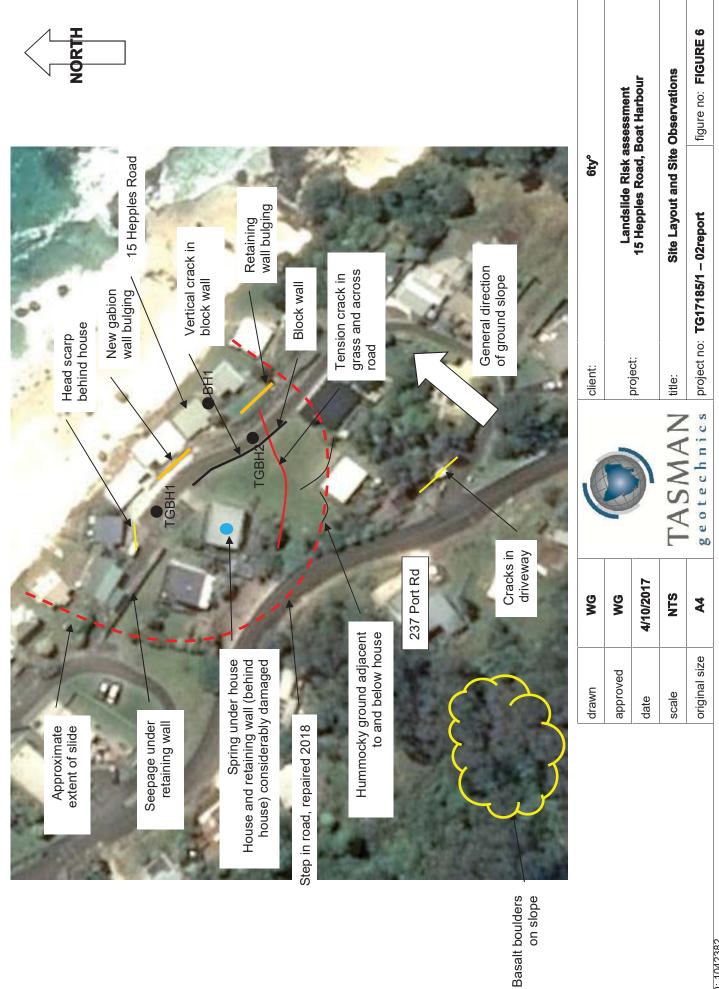
title: MRT Geomorphology Map Extract

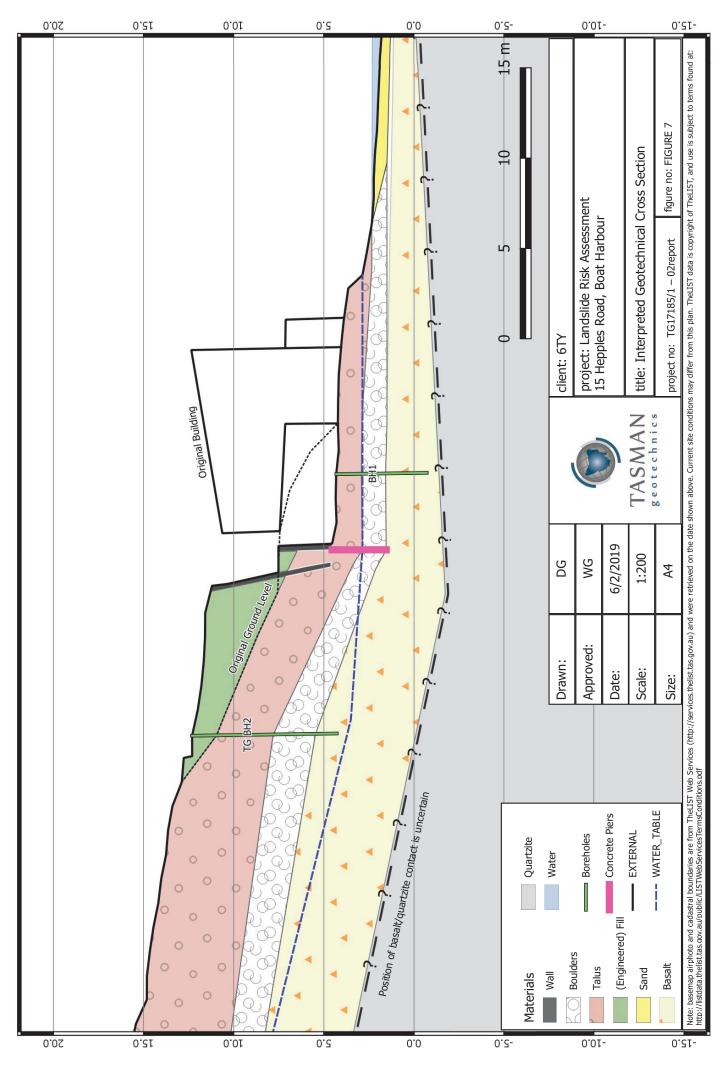
project no: TG17185/1 – 02report figure no: FIGURE 4



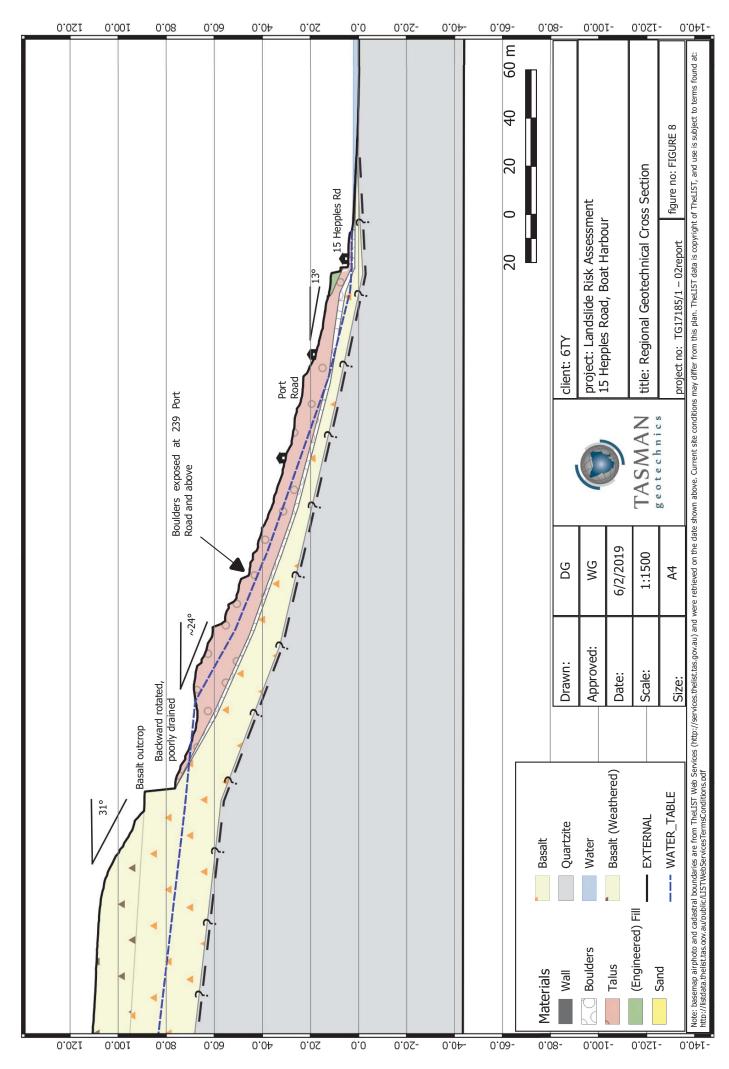


drawn	WG		client:	6ty°			
approved	WG	(60),	project:	Landslide Risk	Landslide Risk Assessment		
date	21/1/2019		project:	15 Hepples Road,	Boat Harbour		
scale	NTS	TASMAN	title:	MRT Landslide Suscept	tibility Map Extracts		
original size	A4	geotechnics	project no:	TG17185/1 – 02report	figure no: FIGURE 5		

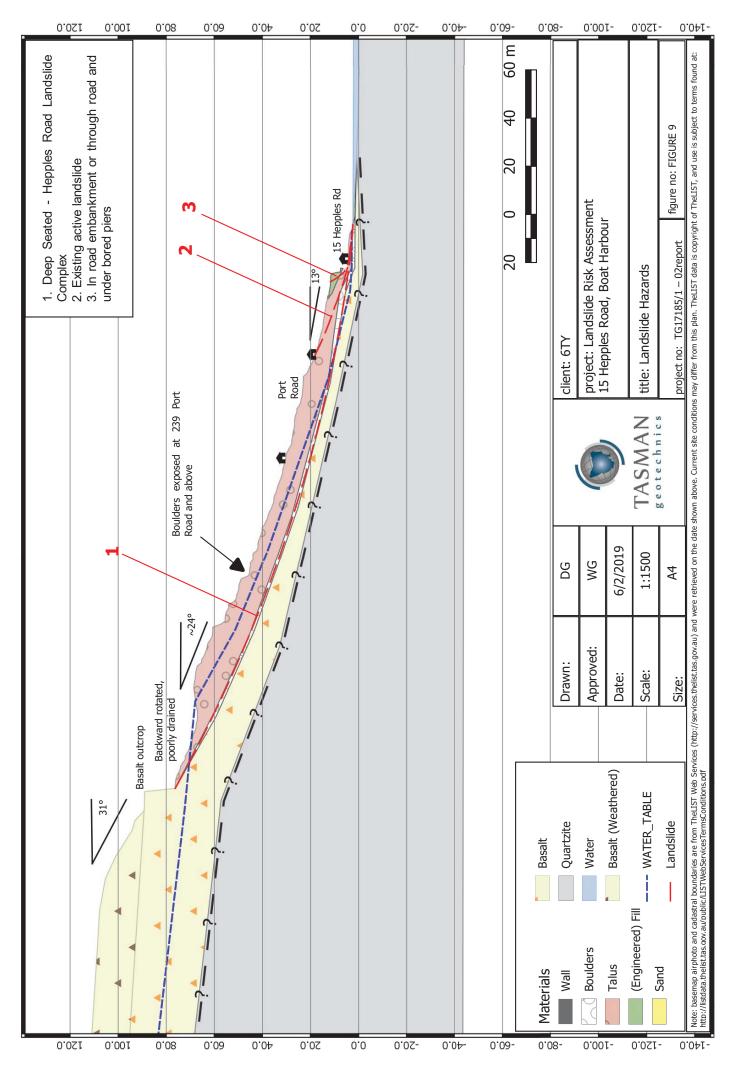




Document Set ID: 1042382 Version: 1, Version Date: 12/04/2019



Document Set ID: 1042382 Version: 1, Version Date: 12/04/2019

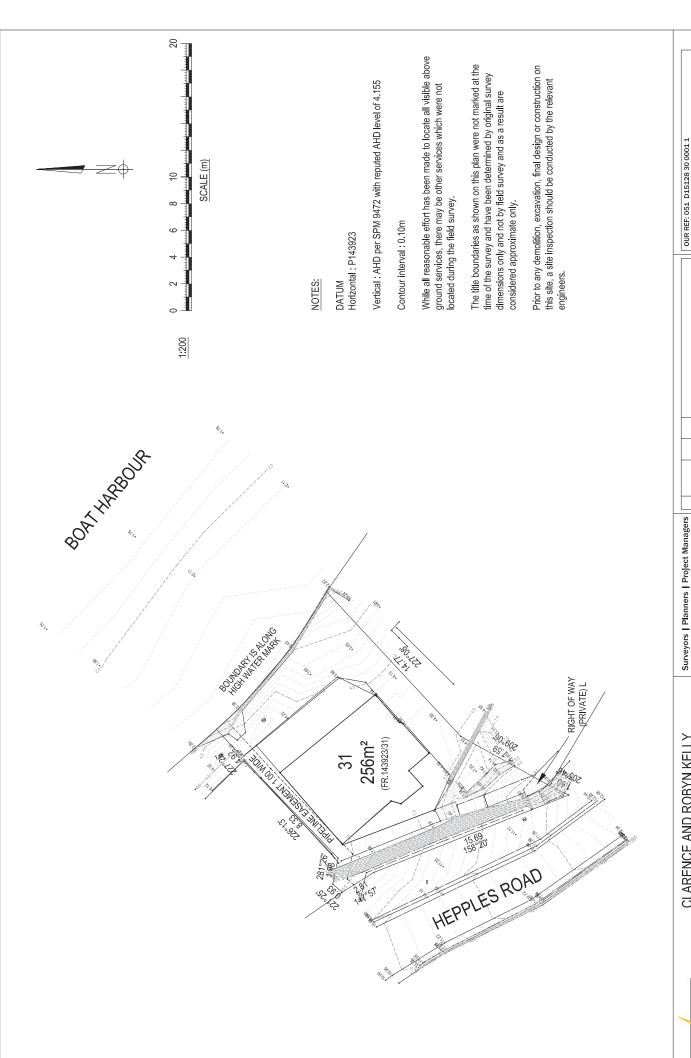


Document Set ID: 1042382 Version: 1, Version Date: 12/04/2019

Appendix ADevelopment Drawings

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01



CLARENCE AND ROBYN KELLY DETAIL SURVEY

LESTER FRANKS

15 HEPPLES ROAD BOAT HARBOUR BEACH TAS 7321

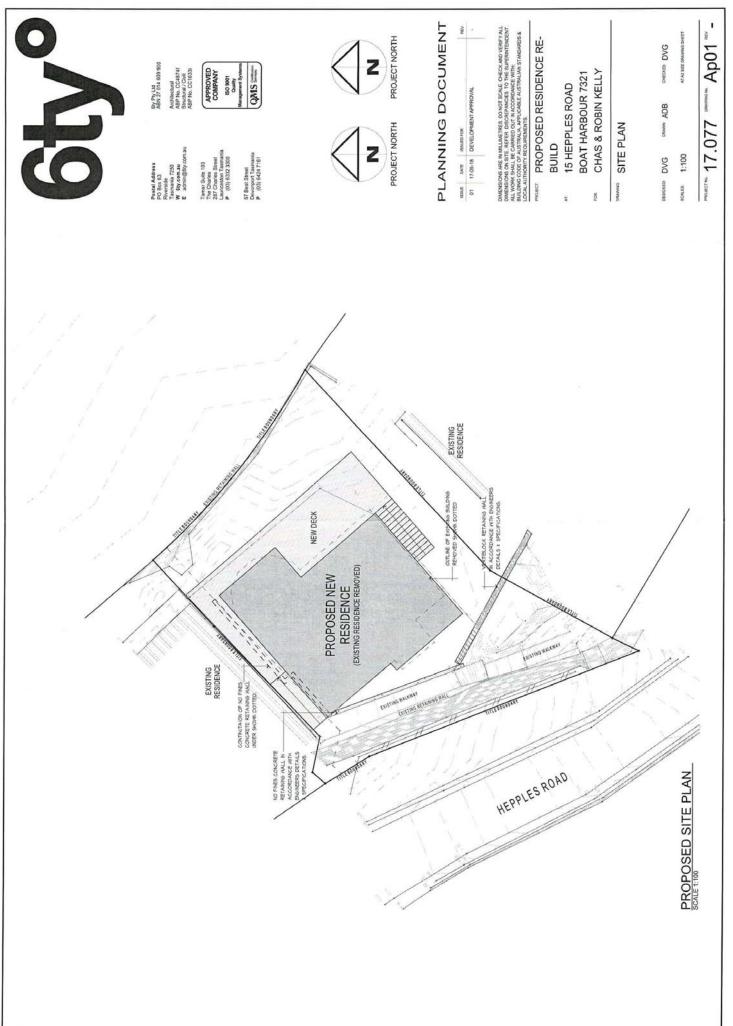
Surveyors | Planners | Project Managers

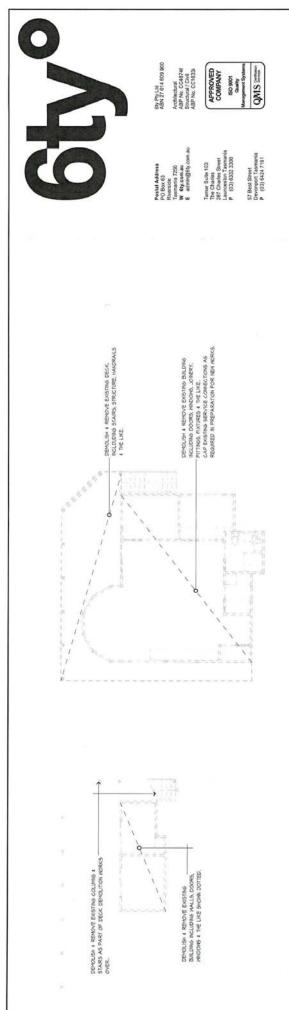
T | 03 6232 0400 F | 03 6231 2844 E | info@lesterfranks.com.au W | www.lesterfranks.com.au A | 2-37 Tasma Street | North Hobart Tasmania 7000

1 28-0
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This plan is

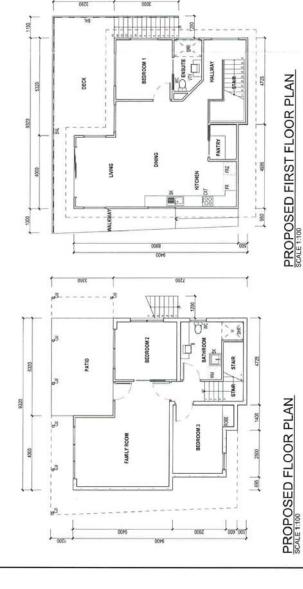
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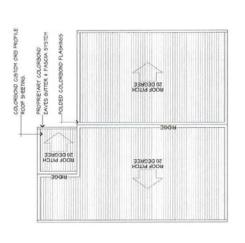
A3





PROPOSED GROUND FLOOR DEMOLITION PLAN PROPOSED FIRST FLOOR DEMOLITION PLAN SCALE 1:100





PROPOSED ROOF PLAN SCALE 1:100

PROPOSED FLOOR PLAN SCALE 1:100

PLANNING DOCUMENT 12-09-18 DEVELOPMENTAPPROVAL

DIMENSIONS ARE IN MILLIMETRES, DO NOT SCALE CHECK AND VERFY ALL MILLIMENSIONS OF RIFE EFFER DISCREPANCES TO THE SUPERNITENDENT, ALL WORK SHALL BE CARREDO OUT IN ACCORDANCE WITH: THORN GODE OF ANSINALA, APPLICABLE AUSTRALIAN STANDARDS & LOCAL AUTHORISTY EQUIPMENTS.

PROPOSED RESIDENCE RE-

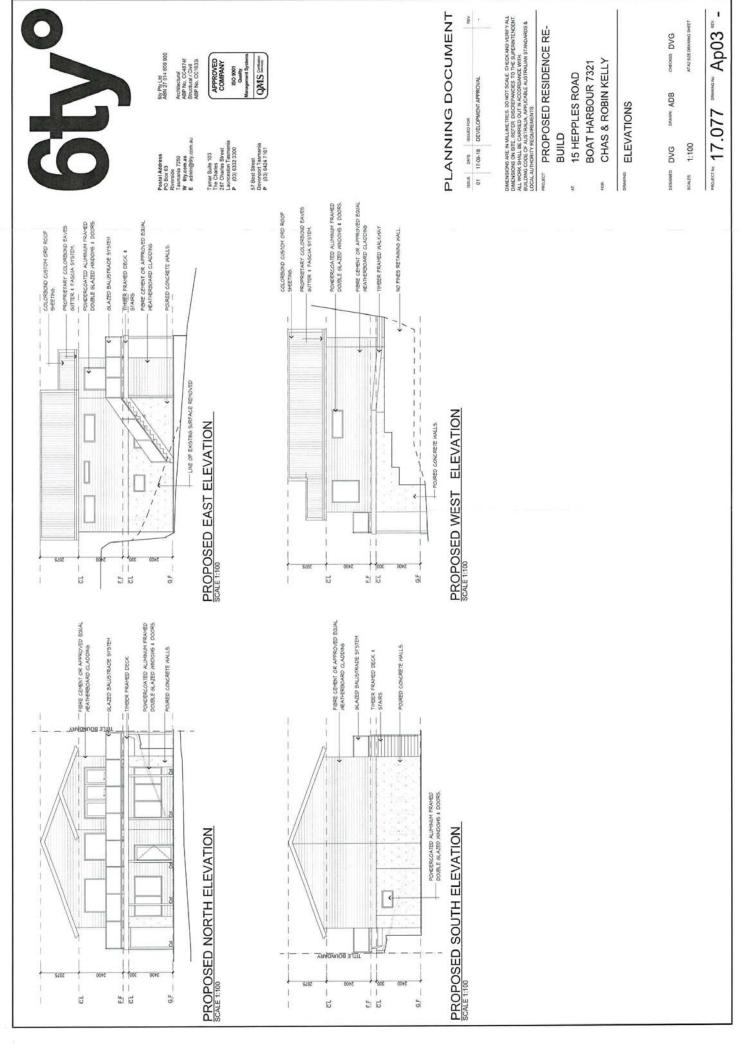
15 HEPPLES ROAD BUILD

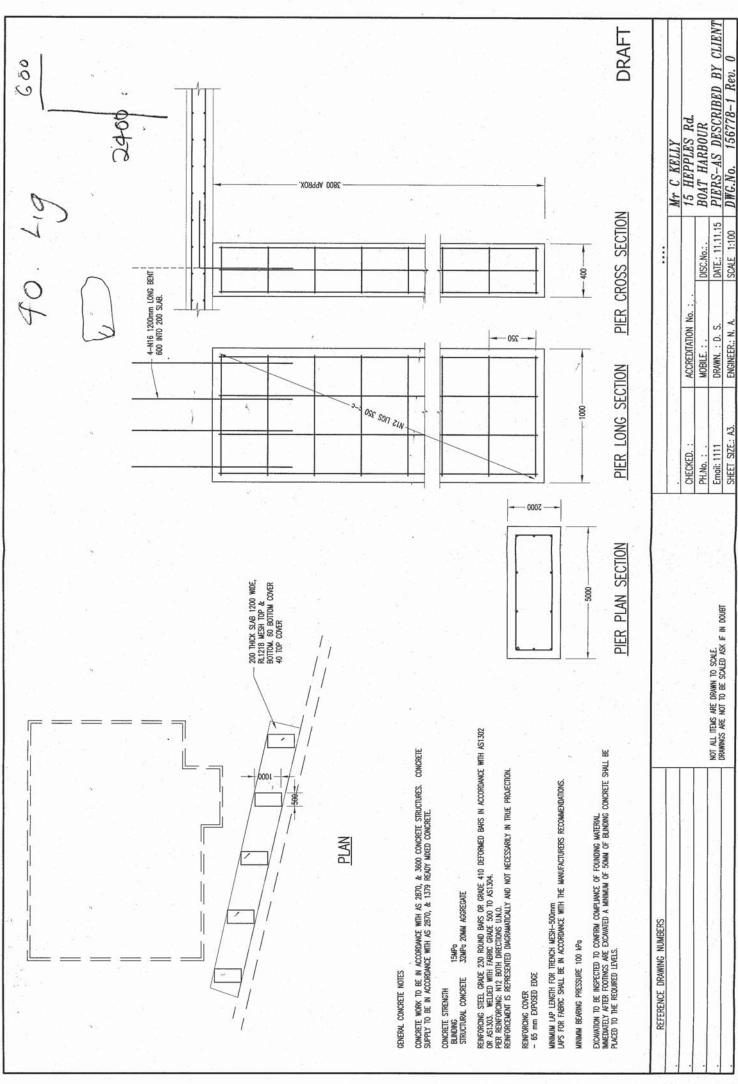
CHAS & ROBIN KELLY BOAT HARBOUR 7321

DEMOLITION, FLOOR & ROOF **PLANS**

ATA2 SIZE DRAWING SHEET CHECKED DAG DRAWN ADB SCALES 1:100 DAG GARDERO

Ap02 ... может» 17.077



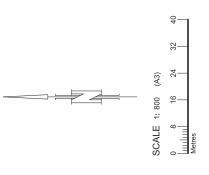


Appendix BLandslip Survey Data

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01





6 Δ to 2009
Northing Displacement Fasting Northing
A to 2004
2009 Northing
Facting
2004 Northing
20 Fasting
Mark Tyne

NOTES:

Date of Survey: 14 September 2016

Horizontal Coordinate Datum is planar based on GDA94, MGA zone 55

Coordinate origin SPM9472, with coordinates (2009) of E: 383593.427 N:5468418.012

If there are a questions relating to the datum of this survey PDA Surveyors should be contacted.

The data shown on this plan was recorded on 13/09/2016 and has been compared to registered surveys P143922 (2004) and SIO159620 (2009). PDA Surveyors accepts no responsibility for the measurements shown on P143922 and SIO159620. Arrows denote the approximate bearing of (D) & (E) displacement.

SIO159620 has been used as the common datum for comparison, with this survey and P143922 both fitted using a Helmert Transformation at (B), (C) & (F). Points (A) and (G) were not observed by SIO159620.

Background imagery is from Google Earth.

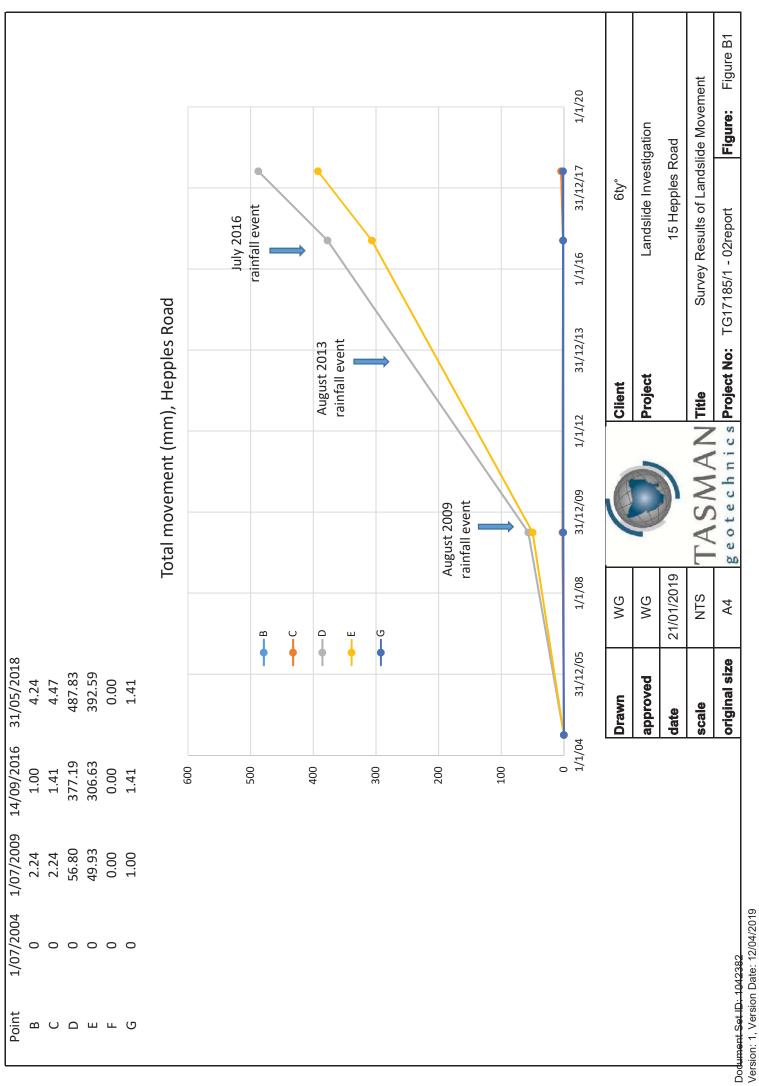
	COORDINALE COMPARISONS	HEPPLES ROAD	BOAT HARBOUR BEACH	× ×	
GEOCINE	B16617	CHECKED	AE	0	SEPTEMBER 2016
SURVEYOR	M	DIRAWN	M	DATE	14 SEPTE
NOTES:					
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(A3)

1: 800

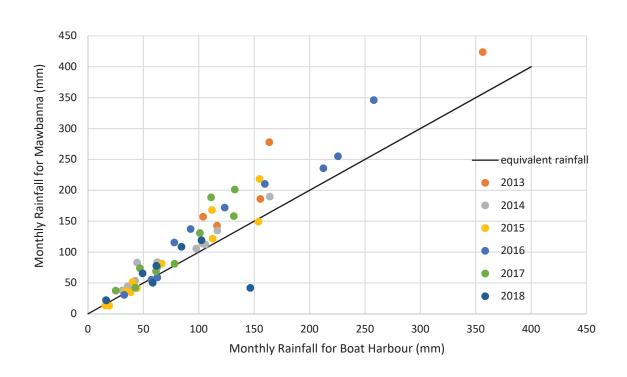
B16617 - 1

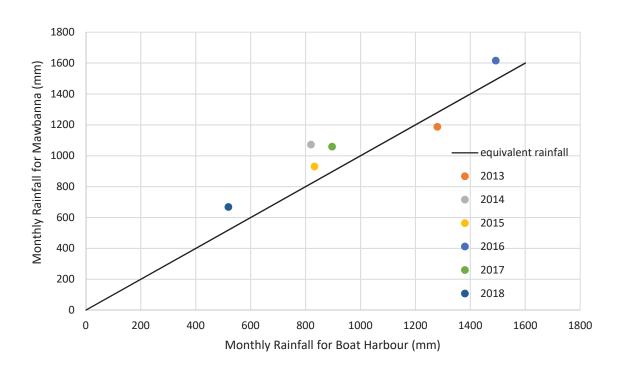


Appendix C Rainfall Data

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01





Drawn	WG		Client	6ty°		
Approved	WG	1	Project	Landslide Invest	tigation	
Date	4/02/2019			15 Hepples R	Road	
Scale	NTS	TASMAN	Title	Rainfall Data Mawbanna a	and Boat I	Harbour
Original size	A4	geotechnics		TG17185/1 - 02report	Figure:	Figure C1

Monthly Rainfall (millimetres)

BOAT HARBOUR

Station Number: 091364 · State: TAS · Opened: 2012 · Status: Open · Latitude: 40.93°S · Longitude: 145.60°E · Elevation: 184 m

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
2012									177.3	31.8	37.7	100.4	
2013	29.8	23.0	59.8	52.0	107.0	38.8	163.7	356.3	155.6	103.8	116.4	73.8	1280.0
2014	35.8	15.9	42.4	103.4	116.7	105.9	164.1	44.3		97.7	30.9	62.4	
2015	41.7	38.4	112.5	19.0	154.8	66.6	153.8	112.0	44.0	15.6	33.8	40.2	832.4
2016	32.6	57.2	62.6	43.9	225.6	212.5	258.0	123.4	159.6	146.8	92.6	77.8	1492.6
2017	61.4	25.0	42.6	78.2	132.4	46.8	111.0	101.0	131.5	85.8	18.5	62.5	896.7
2018	16.5	61.7	84.4	58.4	49.2	102.4		146.5	59.2	37.0	86.9	105.9	

Quality control: 12.3 Done & acceptable, 12.3 Not completed or unknown



Monthly Rainfall (millimetres)

BOAT HARBOUR

Station Number: 091364 · State: TAS · Opened: 2012 · Status: Open · Latitude: 40.93°S · Longitude: 145.60°E · Elevation: 184 m

Statistics for this station calculated over all years of data

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
Lowest	16.5	15.9	42.4	19.0	49.2	38.8	111.0	44.3	44.0	15.6	18.5	40.2	832.4
Highest	61.4	61.7	112.5	103.4	225.6	212.5	258.0	356.3	177.3	146.8	116.4	105.9	1492.6

1) Calculation of statistics

Summary statistics, other than the Highest and Lowest values, are only calculated if there are at least 20 years of data available.

2) Gaps and missing data

Gaps may be caused by a damaged instrument, a temporary change to the site operation, or due to the absence or illness of an observer.

3) Further information

http://www.bom.gov.au/climate/cdo/about/about-rain-data.shtml.

Product code: IDCJAC0001 reference: 44000613 Created on Mon 21 Jan 2019 10:18:42 AM EST



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Monthly Rainfall (millimetres)

MAWBANNA (HARBY HILLS)

Station Number: 091241 · State: TAS · Opened: 1981 · Status: Open · Latitude: 40.97°S · Longitude: 145.37°E · Elevation: 212 m

Year	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
1981				•					•		68.0	43.3	
1982	45.5	52.9	64.4	104.9	137.8		99.8	78.4	133.5				
1983	59.0	4.0	66.0	126.5	91.5	124.5	192.5	154.0	149.0	44.5	84.5	11.1	1107.1
1984	44.0	16.0	122.0	102.0	106.0	18.6	172.8	243.2	157.4	97.8	76.4	135.2	1291.4
1985	70.0	24.6	64.4	74.8	169.5	183.9	121.1	149.4	22.4	132.6	83.6	165.6	1261.9
1986	50.6	34.4	17.6	136.0	97.6	111.0	227.4	104.2	175.1	223.4	58.4	148.2	1383.9
1987	83.2	45.0	75.0	34.4	204.0	107.0	120.4	81.4	82.2	68.2	126.6	72.6	1100.0
1988	27.6	18.4	10.0	79.6	249.0	164.6	258.2	135.2	158.2	245.8	111.1	83.5	1541.2
1989	88.2	25.0	97.4	249.2	137.9	130.2	168.6	75.6	194.0	163.4	40.4	64.2	1434.1
1990	26.0	137.4	44.8	64.4	72.4	154.6	143.8	174.2	121.2	117.6	107.0	81.8	1245.2
1991	84.2	13.8	75.0	75.0	23.6	269.4	189.4	299.0	134.4			58.8	
1992	66.0	57.8	26.4	267.4	163.2	111.0	227.8	199.6	155.0	168.0	150.8	80.0	1673.0
1993	66.8	108.8	64.4	55.6	77.6	90.0	152.8	184.0	94.6	117.2	102.6	175.4	1289.8
1994	89.8	55.6	3.6	83.6	216.2	133.6	170.2	72.6	105.0	102.4	122.6	21.4	1176.6
1995	27.0	45.8	66.2	134.6	84.2	177.0	280.8	138.2	46.0	81.0	65.6	63.4	1209.8
1996	145.2	52.8	133.8	130.6	46.6	211.0	292.4	200.0	206.6	83.2	113.0	53.0	1668.2
1997	115.4	44.0	50.6	59.4	204.8	62.2	91.0	124.6	141.0	69.4	92.8	74.4	1129.6
1998	31.0	63.4	45.0	103.0	89.4	139.2	168.8	104.0		169.4	135.2	81.6	
1999	5.6	111.2	43.4	47.6	193.0	72.8	113.4		92.4	103.4	72.6		
2000	40.4	58.2		88.8	123.0	124.6	242.5	75.6	190.6	127.4	74.4	67.6	
2001	44.4	35.4	145.2	50.4	42.6	173.4	53.2	274.8	173.0	224.8	90.6	71.2	1379.0
2002	74.3	50.8		31.8	83.8	149.6	187.0	160.6	191.6	133.7	50.8	50.4	
2003	65.6	7.4	82.4	131.2	65.0	197.4	185.7	206.2	196.0	79.6	14.4	67.6	1298.5
2004	131.3	31.8	45.8	67.8	153.4	205.6	156.0	129.3	70.1	86.2	100.4	66.2	1243.9
2005	38.0	47.4	29.0	84.8	78.4	108.0	169.4	222.8	141.0	183.8	108.8	147.8	1359.2
2006	38.0	36.4	43.4	145.8	91.9	116.1	125.6	74.4	110.0	54.0	44.0	40.0	919.6
2007	81.5	9.0	51.8	27.2	298.0	54.8	113.0	197.6	164.2	108.0	11.6	113.3	1230.0
2008	9.0	36.8	57.8	73.6	99.0	135.2	171.0	124.6	128.7	28.8	101.2	106.7	1072.4
2009	47.6	11.2	122.6	151.4	131.8	105.4	220.0	331.4	169.0	49.0	78.4	57.6	1475.4
2010	15.0	53.2	123.0	126.0	129.0	152.0	140.6	197.6	180.0	133.6	124.5	149.8	1524.3
2011	199.4	83.6		63.6	53.0		172.4	210.0	89.8	90.2	140.2	46.8	
2012	79.6	78.4	138.8	77.4	114.6	139.2	103.4						
2013							277.9	423.6	186.0	157.2	142.8		
2014	44.6	22.4	53.5	113.6	135.0	112.4	189.8	82.8	91.4	105.6	37.8	83.6	1072.5
2015		35.0	121.6	13.2	218.4	81.2	149.2	168.0	41.8	13.4	36.8	51.5	
2016	30.6	55.2	58.8		255.0	235.6	345.9	172.0	210.4		137.2	115.6	
2017	68.8	37.6	42.2	81.0	201.2	73.8	188.6	130.8	158.2			76.2	
2018	21.8	77.6	108.4	50.1	65.4	119.0	183.4	42.0					

Quality control: 12.3 Done & acceptable, 12.3 Not completed or unknown



Monthly Rainfall (millimetres)

MAWBANNA (HARBY HILLS)

Station Number: 091241 · State: TAS · Opened: 1981 · Status: Open · Latitude: 40.97°S · Longitude: 145.37°E · Elevation: 212 m

Statistics for this station calculated over all years of data

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Annual
Mean	61.6	46.6	69.5	94.5	130.6	133.6	177.5	164.0	137.1	114.9	88.0	82.6	1295.3
Lowest	5.6	4.0	3.6	13.2	23.6	18.6	53.2	42.0	22.4	13.4	11.6	11.1	919.6
5th percentile	13.2	8.6	14.6	30.4	45.6	59.6	98.0	73.9	44.5	36.7	27.8	32.6	1072.4
10th percentile	23.5	12.5	26.9	39.7	59.0	73.1	109.2	75.6	73.7	49.0	38.3	44.0	1080.8
Median	50.6	44.5	64.4	81.0	118.8	127.4	171.0	154.0	145.0	105.6	90.6	72.6	1275.8
90th percentile	105.2	81.0	122.9	141.9	217.3	203.1	266.1	262.2	193.3	183.8	136.8	148.1	1536.1
95th percentile	135.5	109.4	135.8	180.7	250.5	219.6	283.1	308.7	199.7	224.1	141.2	156.1	1649.2
Highest	199.4	137.4	145.2	267.4	298.0	269.4	345.9	423.6	210.4	245.8	150.8	175.4	1673.0

1) Calculation of statistics

Summary statistics, other than the Highest and Lowest values, are only calculated if there are at least 20 years of data available.

2) Gaps and missing data

Gaps may be caused by a damaged instrument, a temporary change to the site operation, or due to the absence or illness of an observer.

3) Further information

http://www.bom.gov.au/climate/cdo/about/about-rain-data.shtml.

Product code: IDCJAC0001 reference: 44059768 Created on Wed 23 Jan 2019 15:10:05 PM EST



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Appendix D

Selected Site Photographs

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01



Photo 1. View of Hepples Road showing damage to kerb and hummocky slope above retaining wall (Sept 2016)



Photo 2. Condition of 15 Hepples Road in Sept 2016

Reference: TG17185/1 - 02report



Photo 3. View of crib wall behind 15 Hepples Road (Sept 2016)



Photo 4. Formwork for strip footing joining bored piers at base of crib wall (image supplied by 6ty°)

Reference: TG17185/1 - 02report



Photo 5. Looking at the site from Hepples Road (sept 2017)



Photo 6. Detail of new construction and old building (sept 2017)

Reference: TG17185/1 - 02report



Photo 7. Verti-block wall at rear of new construction (sept 2017). Note crib wall above verti-blocks

Reference: TG17185/1 - 02report



Photo 8. New no-fines concrete retaining wall (Sept 2017)

Reference: TG17185/1 - 02report



Photo 9. View of site from beach (Sept 2017)



Photo 10. Cut face showing talus (Sept 2017)

Reference: TG17185/1 - 02report



Photo 11. Original (deformed) wall of lower level (Sept 2017)

Reference: TG17185/1 - 02report

Appendix E

Engineering Borehole Logs

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01

ROCK DESCRIPTION EXPLANATION SHEET

Page 1 of 2



The descriptive terms used by Tasman Geotechnics are given below. They are consistent with AS1726-1993

Definitions				
Substance	Effectively homogeneous material, may be isotropic or anisotropic			
Defect	Discontinuity or break in the continuity of a substance or substances			
Mass Any body of material which is not effectively homogenous. It can consists of two or more substances without defective or one or more substances with one or more defects.				
In engineering terms, rock substance is any naturally occuring aggregate of minerals and organics material which cannot be disintegrated or remoulded by hand in air or in water. Other material is described using soil descriptive terms.				

SUBSTANCE DESCRIPTIVE TERMS

Rock Name	Simple rock names are used rather than precise geological classification					
	Coarse grained	0.6mm to 2mm				
Particle Size	Medium grained	0.2mm to 0.6mm				
	Fine grained	0.06mm to 0.2mm				
	Terms for layers or penetrative fabric (e.g. bedding cleavage)					
	Massive	No layering of penetrative fabric				
Fabric	Poorly Developed	Layers or fabric just visible. Little effect on properties.				
	Well Developed	Layering or fabric distinct. R breaks more easily parallel t layering or fabric.				

BLOCK SHAPE TERMS

Blocky	Approximately equidimensional
Tabular	Thickness much less than length or width
Columnar	Height much greater than cross section

ROCK SUBSTANCE STRENGTH TERMS

TO SIX SOL	0174	101 011111	OTT TEIUMO
Term	Abbreviation	Point Load Index, Is ₅₀ (MPa)	Field Guide to Strength
Very Low	VL	<0.1	Material crumbles under firm blows with sharp end of pick; can be peeled with knife; too hard to cut a triaxial sample by hand. Pieces up to 30m thick can be broken by finger pressure.
Low	L	0.1 to 0.3	Easily scored with a knife; indentation 1mm to 3mm show in the specimen with firm blows of the pick point; has dull sound under hammer. A piece of core 150mm long by 50mm diameter may be broken by hand. Sharp edges of core may be friable and break during handling
Medium	М	0.3 to 1	Readily scored with a knife; a piece of core 150mm long by 50mm diameter can be broken by hand with difficulty.
High	Н	1 to 3	A piece of core 150mm long by 50mm diameter can not be broken by hand but can be broken by a pick with a single firm blow; rock rings under hammer.
Very High	VH	3 to 10	Hand specimen breaks with pick after more than one blow; rock rings under hammer.
Extremely High	EH	>1	Specimen requires many blows with geological pick to break through intact material; rock rings under hammer

ROCK DESCRIPTION EXPLANATION SHEET

Page 2 of 2



CLASSIFICATION OF WEATHERING PRODUCTS

Term	Abbreviation	Definition
Residual Soil	RS	Soil derived from the weathering of rock; the mass structure and substance fabric are no longer evident; there is a large change in volume but the soil has not been significantly transported.
Extremely Weathered	XW	Material is weathered to such an extent that it has soil properties, ie, it either disintegrates or can be remoulded in water. Fabrix of original rock still visible.
Distinctly Weathered	DW	Rock strength usually changed by weathering. The rock may be highly discoloured, usually by iron staining. Porosity may be increased by leaching, or may be decreased due to deposition of weathering products in pores.
Slightly Weathered	SW	Rock is slightly discoloured but shows little or no change of strength from fresh rock.
Fresh	FR	Rock shows no signs of decomposition or staining.

COMMON DEFECTS IN ROCK MASSES

COMMON DEFECTS IN	
Term	Definition
Parting	A surface or crack across which the rock has little or no tensile strength. Parallel or sub parallel to layering or a planar anisotropy in the rock substance. May be open or closed.
Joint	A surface or crack across which the rock has little or no tensile strength but which is not parallel or sub parallel to layering or planar anisotropy in the rock substance. May be open or closed.
Sheared Zone	Zone of rock substance with roughly parallel near planar, curved or undulating boundaries cut by closely spaced joints, sheared surfaces or other defects. Some of the defects are usually curbed and intersect to divide the mass into lenticular or wedge shaped blocks.
Sheared Surface	A near planar, curved or undulating surface which is usually smooth, polished or slickensided.
Crushed Seam	Seam with roughly parallel almost planar boundaries, composed of disoriented, usually angular graments of the host rock substance which may be more weathered than the host rock. The seam has soil properties.
Infilled Seam	Seam of soil substance usually with distinct roughly parallel boundaries formed by the migration of soil into an open cavity or joint. Infilled seams less than 1mm thick may be described as veneer or coating on joint surface.
Extremely Weathered Seam	Seam of soil substance, often with gradational boundaries. Formed by weathering of the rock substance in places.

DEFECT ROUGHNESS TERMS

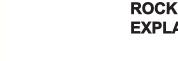
221 201 10000111	1200 12111110
Slickensided (SI)	Grooved or stiated surface; usually polished
Polished (Po)	Shiny smooth surface
Smooth (Sm)	Smooth to touch; few or no surface irregularites
Rough (Ro)	Many small surface irregularites (amplitude generally less than 1mm); feels like fine to coarse sandpaper
Very Rough (VR)	Many large surface irregularities (amplitude generally more than 1mm); feels like, or coarser than, very coarse sandpaper

DEFECT COATING TERMS

DEI EOI C	DEI EGI GOATING TERMING						
Clean (CI)	No visible coating						
Stained (St)	No visible coating but surfaces are discoloured						
Veneer (Ve)	A visible coating of soil or mineral too thin to measure; may be patchy						
Coating (Co)	A visible coating up to 1mm thick. Thicker soil material is described using appropriate defect terms (e.g. infilled seam). Thicker rock strength material is usually described as a vein.						

DEFECT SHAPE TERMS

Planar (PI)	The defect does not vary in orientation
Curved (Cu)	The defect has a gradual change in orientation
Stepped (Sp)	The defect has one or more well defined steps
Irregular (Ir)	The defect has many sharp changes in orientation
Undulating (Un)	The defect has a wavy surface



ROCK DESCRIPTION EXPLANATION SHEET



Soils are described in accordance with the Unified Soil Classification System (USCS), as shown in the following table.

FIELD IDENTIFICATION

	m is	/ELS	GW	Well graded gravels and gravel-sand mixtures, little or no fines
S	n 63mm	GRAVELS	GP	Poorly graded gravels and gravel-sand mixtures, little or no fines
SOILS	less than 75mm	VELL	GM	Silty gravels, gravel-sand-silt mixtures, non- plastic fines
GRAINED	ial 0.0	GRAVELL Y SOILS	GC	Clayey gravels, gravel-sand-clay mixtures, plastic fines
	of material ler than 0.0	SANDS	SW	Well graded sands and gravelly sands, little or no fines
COARSE	65% of larger	SAN	SP	Poorly graded sands and gravelly sands, little or no fines
Ö	than	ILS	SM	Silty sand, sand-silt mixtures, non-plastic fines
	more	SANDY SOILS	SC	Clayey sands, sand-clay mixtures, plastic fines

	1			DRY STRENGTH	DILATANCY	TOUGHNESS
	al less 075mm CLAY, mit less 50%	ML	Inorganic silts, very fine sands or clayey fine sands	None to low	Quick to slow	None
SOILS	.≝ 0. ∞ :≡ ⊏	CL	Inorganic clays or low to medium plasticity, gravelly clays, sandy clays and silty clays	Medium to high	None to very slow	Medium
	ss than SILT liquid that	OL	Organic silts and organic silty clays of low plasticity	Low to medium	Slow	Low
GRAINED	35% is le /// /// /// it an	МН	Inorganic silts, micaceous or diatomaceous fine sands or silts	Low to medium	Slow to none	Low to medium
FINE	63m 63m 7 & C uid I	СН	Inorganic clays of high plasticity, fat clays	High	None	High
	than 6%	ОН	Organic clays of medium to high plasticity	Medium to high	None to very slow	Low to medium
	PEAT	Pt	Peat muck and other highly organic soils			

Particle size descriptive terms

	aooop	
Name	Subdivision	Size
Boulders		>200mm
Cobbles		63mm to 200mm
Gravel	coarse	20mm to 63mm
	medium	6mm to 20mm
	fine	2.36mm to 6mm
Sand	coarse	600μm to 2.36mm
	medium	200μm to 600μm
	fine	75μm to 200μm

Moisture Condition

Dry (D)	Looks and feels dry. Cohesive soils are hard,
	friable or powdery. Granular soils run freely
	through fingers.
Moist (M)	Soil feels cool, darkened in colour. Cohesive
	soils are usually weakened by moisture
	presence, granular soils tend to cohere.
Wet (W)	As for moist soils, but free water forms on
	hands when sample is handled

Cohesive soils can also be described relative to their plastic limit, ie: <Wp, =Wp, >Wp

The plastic limit is defined as the minimum water content at which the soil can be rolled into a thread 3mm thick.

Consistency of cohesive soils

Terr	m	Undrained	Field guide
1611	11	strength	i leid guide
Very sof	t VS	<12kPa	A finger can be pushed well into soil with little effort
Soft	S	12 - 25kPa	Easily penetrated several cm by fist
Firm	F	25 - 50kPa	Soil can be indented about 5mm by thumb
Stiff	St	50-100kPa	Surface can be indented but not penetrated by thumb
Very stiff	VSt	100-200kPa	Surface can be marked but not indented by thumb
Hard	Н	>200kPa	Indented with difficulty by thumb nail
Friable	Fb	-	Crumbles or powders when scraped by thumb nail

Density of granular soils

Term	Density index					
Very loose	<35%					
Loose	15 to 35%					
medium dense	35 to 65%					
Dense	65 to 85%					
Very dense	>85%					

Minor Components

	inpondito	
Term	Proportions	Observed properties
Trace of	Coarse grained: <5%	Presence just detectable by feel or eye. Soil
	Fine grained: <15%	properties little or no different to general
		properties of primary component.
With some	Coarse grained: 5-12%	Presence easily detected by feel or eye. Soil
	Fine grained: 15-30%	properties little different to general properties of
		primary component.

ENGINEERING CORED BOREHOLE LOG

Client : 6TY Project : LRA

Location: 15 Hepples Road

Boat Harbour



Borehole no. BH1

Sheet no. 1 of 1 **Job no.** TG17185/1

Date: 21/09/2017

Logged By: AC

Drill model: Posi Trak SR-70 ASVSlope:degRL Surface:Barrel type: NQTTfluid: mudBearing:degDatum:

		Dr	Iling inform	ation			Rock substance						Т				Rock mass defects
Method	Case-lift	Water	Notes Samples Tests	J.		Graphic Log	Substance Description rock type, grain characteristics, colour, structure, minor components	Weathering			(50)		Spa (n	efectacir nm)	t ig	Defect Description thickness, type, inclination,
_							TALLIO I I I I I I I I I I I I I I I I I I			∠∠	Ι	¥Ξ	33	9	30	<u> </u>	particular general
auger					1.00	4 0 4 0	TALUS, baslatic clay matrix with cobbles and gravel of basaltic origin										
TTON					2.00	4 0 0	Auger refusal @ 1.3m BASALT, cobbles and boulders, slightly weathered, clay infill										
					3.00		BASALT, black, highly fractured, iron staine fractures and some calcite veining	-									horizontal fractures
	•				4.00	V V V V V V V V V V V V V V V V V V V							ŀ				horizontal and 45° fractures
					5.00	V V V V V V V V V											
					6.00 	•	Terminated @ 5.0m										



Drawn	ЕО		Client	6TY		
approved	MG		Project	Landslide Risk Assessment	essment	
date	20/12/2017			15 Hepples Road, Boat Harbour	at Harbour	
scale	NTS	TASMAN Title	Title	Core Photo	0	
original size	A4	geotechnics Project No: TG17185/1-01report	Project No:	TG17185/1 - 01report	Figure:	Figure: Figure BH1

ENGINEERING CORED BOREHOLE LOG

Client: Waratah Wynyard Council Project: Landslide Investigation Location: Hepples Road, Boat Harbour



Borehole no. TGBH1

Sheet no. 1 of 1 **Job no.** TG16160/1

Date: 8/09/2016 **Logged By:** EB

Drill model : Gemco Slope : deg RL Surface : Barrel type : HQTT fluid: mud Bearing : deg Datum :

		Dri	Iling inform	ation			Rock substance						Т					Rock mass defects
Method	Case-lift	Water	Notes Samples Tests	Water		Graphic Log	Substance Description rock type, grain characteristics, colour, structure, minor components	Weathering			(50))	30	S _I	(mr	ing		Defect Description thickness, type, inclination, planarity, roughness, coating particular general
HQTT Auger			50% recovery U63 80% recovery 100% recovery 50% recovery recovery		1.00 2.00 2.00 3.00 4.00 5.00	V V V V V V V V V V V V V V V V V V V	FILL: SAND, fine to medium grained, light brown, with some coarse, angular gravel FILL: SANDY GRAVEL, coarse grained, angular, orange FILL: GRAVEL, coarse grained TALUS: BASALT BOULDERS in GRAVELLY CLAY matrix, high plasticity clay, brown/grey, firm to stiff clay RESIDUAL SOIL (BASALT), presenting as GRAVELLY CLAY, medium plasticity, black/dark red, angular gravel BASALT, fine grained, massive, brown/blue BASALT, fine grained, massive, dark blue	RS										no water return 3.5 to 3.6m Sub-vertical joint set (30deg to 50deg to core axis): undulating, rough, clay filled Vertical joint: undulating, rough, clean also: horizontal joints, rough, undulating, clean
					8.00				L	Ш		Ш		Ш			\perp	





drawn	WG
approved	WG
date	8/3/2017
scale	NTS
original size	A4



client:	Waratah W	/ynyard Council
project:		e Investigation ad, Boat Harbour
title:	TGBH1 Co	re Photographs
project no: TG16160/1	– 01report	figure no: FIGURE TGBH1

ENGINEERING CORED BOREHOLE LOG

Client: Waratah Wynyard Council Project: Landslide Investigation Location: Hepples Road, Boat Harbour



Borehole no. TGBH2

Sheet no. 1 of 1 **Job no.** TG16160/1

Date: 8/09/2016 **Logged By:** EB

Drill model : GemcoSlope :degRL Surface :Barrel type : HQTTfluid: mudBearing :degDatum :

		Dri	Iling inform	ation		Ι	Rock substance							Rock mass defects					
						D.		_	T	C,	pa -	.~41	h		De	fec			
р	≝	٦	Notes	٦.		Graphic Log	Substance Description	Weathering			rer s(5				Spa	acin	g	Defect Description thickness, type, inclination	n
Method	Case-lift	Water	Samples	Water		phic	rock type, grain characteristics, colour,	athe								nm)		planarity roughness soot	ing
Σ	ပိ	>	Tests	>		Grap	structure, minor components	We						30 300 1000 1000		80			
L	<u> </u>					Ŭ					∑:	ιş	品	30	9 9	30	- X	particular gene	ral
HQTT					_		FILL: GRAVELLY SAND, fine grained, white					ı							
Ĭ					_		Wille					ı							
			no		_							ı							
			recovery			4						ı							
					1.00	ł						ı							
	┝╼				_							ı							
					_		TALUS: BOULDERS in GRAVELLY CLAY		ł	H	Н	+	+	+	╀	H	Н		
			no		_		matrix, high plasticity, reddish brown, soft					ı							
			recovery		2.00	1	to firm clay					ı							
	∳ -•				2.00	1						ı							
					_	-													
			000/		_	1													
			80% recovery		_	1						ı							
			10001019		3.00	1						ı							
	T				0.00	1						ı							
			100%		_	1						ı							
			recovery		_	1						ı							
					_	1						ı							
					4.00	1						ı							
			75%			1						ı							
			recovery		_	1						ı							
	•				_	1						ı							
						1						ı							
			25%		5.00							ı							
			recovery									ı							
	∳ -•]													
			100%									ı							
	∳ -•		recovery		_	V V V	RESIDUAL SOIL (BASALT), presenting as	PS	t	H	Н	+	H	+	╁	H	H		
			100%		6.00	l v v	CLAYEY GRAVEL, red/black/brown,	110				ı							
			recovery		_	vvv	angular				Ц	ı							
	•				_	v v v						ı							
			80%		_	V V					Ц	Т							
	••		recovery		_	V V V		<u> </u>	Ļ	\perp	Ц	L	L		L	$oxed{oxed}$	Ц		
					7.00	٧٧	BASALT, fine grained, massive, dark blue	DW			Ш								
			100%		_	v v v					Ш								
			recovery		_	v v					Ш				Г				
					_	v v v					Ш								
					_	V V					П								
	1				8.00	V V V					Ш								

Terminated at 8.0m





drawn	WG
approved	WG
date	8/3/2017
scale	NTS
original size	A4



client:	Waratah W	ynyard Council
project:		Investigation d, Boat Harbour
title:	TGBH2 Cor	re Photographs
project n	o: TG16160/1 - 01report	figure no: FIGURE TGBH2

Appendix F

Laboratory Test Certificate

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01

Head Office 25 Metcalf Street
DANDENONG SOUTH VIC 3175

Ph: +61 3 8796 7900 Fax: +61 3 8796 7944



Undrained Triaxial Test with measurement of pore water pressure

Customer: Tasman Geotechnics Pty Ltd

Report Number: 1000572 Report Date: 28/09/2016

Customer Address: PO Box 4026, Invermay, Tasmania 7248

Project: Hepples Road, Boat Harbour

Request No: -

Location: Tasmania

Test Method: AS1289.6.4.2

-1

Customer Order No: TG16160/1

Page: 1 of 5

Testing performed and reported at our Dandenong South Laboratory

Sample No.: 1610775 Test method: AS1289.6.4.2

Borehole: BH01 Normal Stress: 25, 50, 100

Depth: 2.45 - 2.95m

Pore pressure: 600

Sample Date: 12/09/2016

Sample dimensions (mm): 63 x 127mm

Sample Type: U63 Date tested: 19 - 24/09/2016

Results Summary

Dry density (t/m³): 1.39

0 Cohesion c':

Initial Moisture content (%)

34.0

Angle of shear resistance Φ':

Final Moisture content (%) 39.3 Mode of failure: no visible failure mode

Axial strain rate: Strain at failure: Minor stress Ó_{3f} Major Stress Ó1_f Corr Dev Stress

Stage 1	Stage 2	Stage 3
0.02	0.02	0.02
0.38	0.6	1.5
13	26	47
26.9	68.7	131.4
14	43	84

Failure criteria: Max Stress Ratio

Remarks:

Page 1 of 5





Accredited for compliance with ISO/IEC 17025. The results of tests, calibrations and/or measurements included in this document are traceable to Australian/national standards.

APPROVED SIGNATORY

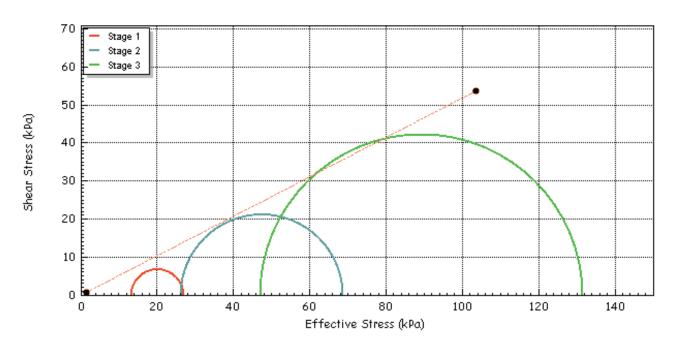
orm No.: CG336.000 ue Date: 19/02/2013

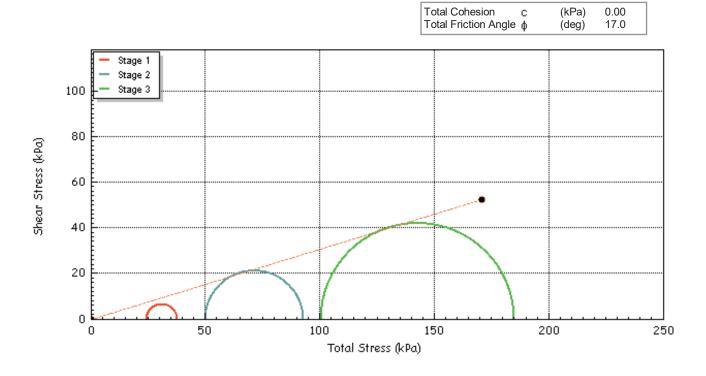
Effective Stress Triaxial Compression

Consolidated Undrained

Shear Stage Plots

Effective Cohesion	c'	(kPa)	0.00
Effective Friction	φ'	(deg)	27.4





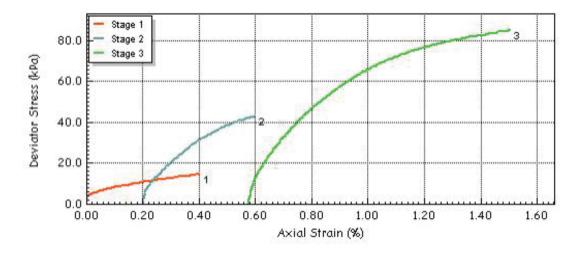
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	Site Reference		Test Date 1			19/09/2016		
	Jobfile Hepples Road Boat Harbour				Sample	mple 1610775		
CHADWICK	Client	Tasman Geotechn	nics		Borehole	BH01 2.45	- 2.95m	
GEOTECHNICS	Operator	TRA	Checked	ARC	C	Approved	ARCC	

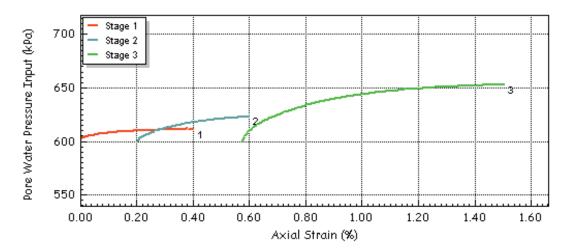
Dandenong South - NATA 12719

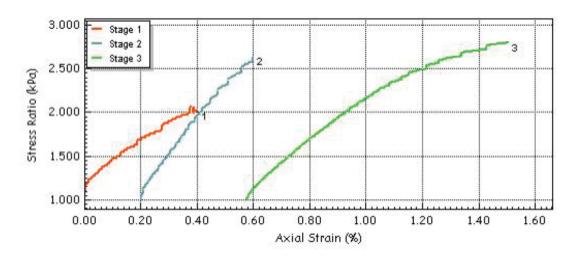
Effective Stress Triaxial Compression

Consolidated Undrained

Shear Stage Plots







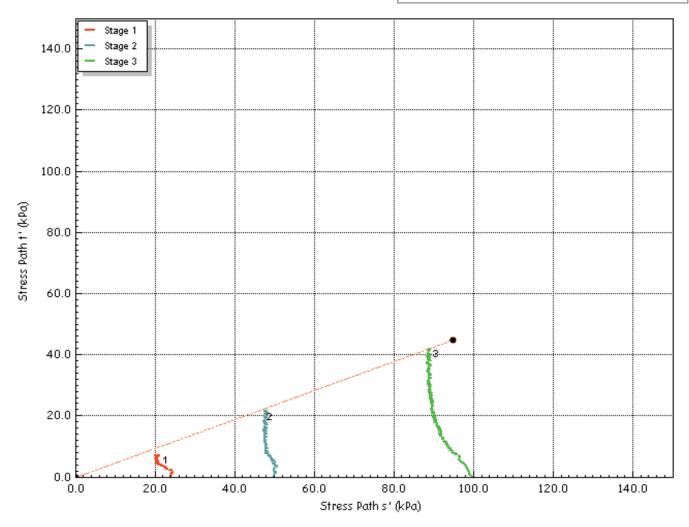
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	Site Reference	1000572			Test Date	19/09/2016	
	Jobfile	Hepples Road Boa	Harbour		Sample	1610775	
CHADWICK	Client	Tasman Geotechn	ics		Borehole	BH01 2.45	- 2.95m
GEOTECHNICS	Operator	TRA	Checked	ARC	C	Approved	ARCC

Dandenong South - NATA 12719

Consolidated Undrained

Shear Stage Plots

Effective Cohesion	c'	(kPa)	0.00
Effective Friction Angle	φ'	(deg)	28.2
Stress Path Intercept	to'	(kPa)	0.00
Stress Path Inclination	θ	(deg)	25.3



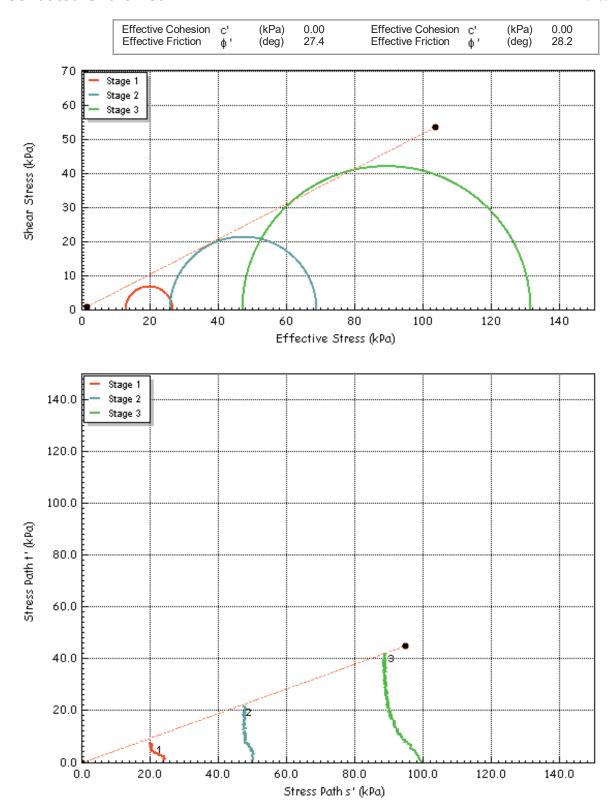
	Test Method	AS1289.6.4.2 - 199	98		Test Name Database: .\SQLI	CUPP 0775 EXPRESS \ Ch	
	Site Reference	1000572			Test Date	19/09/2016	
	Jobfile	Hepples Road Boa			Sample	1610775	
CHADWICK	Client	Tasman Geotechn	ics		Borehole	BH01 2.45	5 - 2.95m
GEOTECHNICS	Operator	TRA	Checked	ARC	C	Approved	ARCC

Dandenong South - NATA 12719

Effective Stress Triaxial Compression

Consolidated Undrained

Shear Stage Plots



	Test Method	AS1289.6.4.2 - 19	98		Test Name Database: .\SQLI	CUPP 0775 EXPRESS \ Cha	
	Site Reference	Site Reference 1000572			Test Date	19/09/2016	
	Jobfile	Jobfile Hepples Road Boa			Sample	1610775	
CHADWICK	Ollotti	Tasman Geotechr	nics		Borehole	BH01 2.45	- 2.95m
GEOTECHNIC	Operator	ΓRA	Checked	ARC	C	Approved	ARCC

Dandenong South - NATA 12719

Appendix G Landslide Risk Matrix

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01



Terminology for use in Assessing Risk to Property

These notes are provided to help you understand concepts and terms used in Landslide Risk Assessment and are based on the "Practice Note Guidelines for Landslide Risk Management 2007" published in *Australian Geomechanics* Vol 42, No 1, 2007.

Likelihood Terms

The qualitative likelihood terms have been related to a nominal design life of 50 years. The assessment of likelihood involves judgment based on the knowledge and experience of the assessor. Different assessors may make different judgments.

Approximate Annual Probability	Implied indicative Recurrence Interval	Description	Descriptor	Level
10 ⁻¹	10 years	The event is expected to occur over the design life	Almost Certain	Α
10 ⁻²	100 years	The event will probably occur under adverse conditions over the design life	Likely	В
10 ⁻³	1000 years	The event could occur under adverse conditions over the design life	Possible	С
10 ⁻⁴	10,000 years	The event might occur under very adverse conditions over the design life	Unlikely	D
10 ⁻⁵	100,000 years	The event is conceivable but only under exceptional circumstances over the design life	Rare	E
10 ⁻⁶	1,000,000 years	The event is inconceivable or fanciful for the design life	Barely Credible	F

Qualitative Measures of Consequence to Property

Indicative Cost of Damage	Description	Descriptor	Level
200%	Structure(s) completely destroyed and/or large scale damage requiring major engineering works for stabilisation. Could cause at least one adjacent property major consequential damage.	Catastrophic	1
60%	Extensive damage to most of structure, and/or extending beyond site boundaries requiring significant stabilisation works. Could cause at least one adjacent property medium consequential damage	Major	2
20%	Moderate damage to some of structure, and/or significant part of site requiring large stabilisation works. Could cause at least one adjacent property minor consequential damage.	Medium	3
5%	Limited damage to part of structure, and/or part of site requiring some reinstatement stabilisation works	Minor	4
0.5%	Little damage.	Insignificant	5

The assessment of consequences involves judgment based on the knowledge and experience of the assessor. The relative consequence terms are value judgments related to how the potential consequences may be perceived by those affected by the risk. Explicit descriptions of potential consequences will help the stakeholders understand the consequences and arrive at their judgment.

TASMAN GEOTECHNICS Rev 01, June 2008

Qualitative Risk Analysis Matrix – Risk to Property

Likelihood		Consequences to Property					
	Approximate annual probability	1: Catastrophic	2: Major	3: Medium	4: Minor	5: Insignificant	
A: Almost Certain 10 ⁻¹		VH	VH	VH	Н	L	
B: Likely	B: Likely 10 ⁻²		VH	Н	M	L	
C: Possible 10 ⁻³		VH	Н	M	M	VL	
D: Unlikely 10 ⁻⁴		Н	M	L	L	VL	
E: Rare 10 ⁻⁵		M	L	L	VL	VL	
F: Barely credible 10 ⁻⁶		L	VL	VL	VL	VL	

NOTES:

- 1. The risk associated with Insignificant consequences, however likely, is defined as Low or Very Low
- 2. The main purpose of a risk matrix is to help rank risks and set priorities and help the decision making process.

Response to Risk

In general, it is the responsibility of the client and/or regulatory and/or others who may be affected to decide whether to accept or treat the risk. The risk assessor and/or other advisers may assist by making risk comparisons, discussing treatment options, explaining the risk management process, advising how others have reacted to risk in similar situations and making recommendations. Attitudes to risk vary widely and risk evaluation often involves considering more than just property damage (eg environmental effects, public reaction, business confidence etc).

The following is a guide to typical responses to assessed risk.

R	isk Level	Example Implications				
VH	Very High	Unacceptable without treatment. Extensive detailed investigation and research, planning and implementation of treatment options essential to reduce risk to Low; may be too expensive and not practical. Work likely to cost more than the value of the property.				
Н	High	Unacceptable without treatment. Detailed investigation, planning and implementation of treatment options required to reduce risk to Low. Work would cost a substantial sum in relation to the value of the property.				
М	Moderate	May be tolerated in certain circumstances (subject to regulator's approval) but requires investigation, planning and implementation of treatment options to reduce the risk to Low. Treatment options to reduce to Low risk should be implemented as soon as practicable.				
L	Low	Usually accepted by regulators. Where treatment has been required to reduce the risk to this level, ongoing maintenance is required.				
VL	Very Low	Acceptable. Manage by normal slope maintenance procedures				

TASMAN GEOTECHNICS Rev 01, June 2008

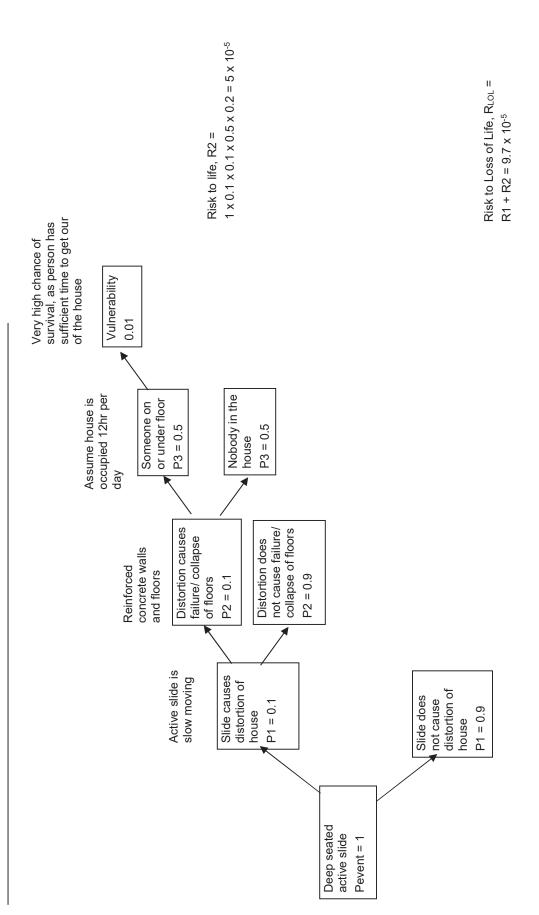
Appendix H Risk to Life

Tasman Geotechnics

Reference: TG17185/1 - 02report Rev01

 $0.02 \times 0.8 \times 0.9 \times 0.1 \times 0.33 \times 0.1 = 4.7 \times 10^{-5}$ Risk to life, R1 = High chance of survival Vulnerability Back half of house occupied of house occupied Assume back half Back half of house un-P4 = 0.33P4 = 0.67occupied 8hr per day Reinforced concrete walls Event Tree - Risk to Life, with management measures where recommended Outside wall Outside wall collapses P3 = 0.9P3 = 0.1stays Collapsed retaining wall impacts house close to house impact house wall does not Collapsed Wall very P2 = 0.9P2 = 0.1retaining wall Slide causes collapse of retaining wall collapse of Estimated Slide does not cause P1 = 0.8P1 = 0.2Medium scale Pevent = 0.02landslide

Tasman Geotechnics Reference: TG17185/1 - 02report



Tasman Geotechnics Reference: TG17185/1 - 02report

Our Ref: 17.077

Measured form and function



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11 April 2019

Ms Rebecca Plapp
Town Planner
Waratah Wynyard Council

By Email: rplapp@warwyn.tas.gov.au

Dear Rebecca,

<u>SUPPORTING INFORMATION - HAZARD MANAGEMENT CODE (E6) - DA 53/2018 - 13 AND 15 HEPPLES ROAD, BOAT HARBOUR</u>

Thank you for the opportunity to provide further information in support of development application DA 53/2018 prior to the commencement of the public exhibition period.

The purpose of this letter is to provide an analysis of the Landslide Risk Assessment prepared by Tasman Geotechnics against the applicable standards of the Hazard Management Code.

In preparing the Landslip Risk Assessment (LRA), Tasman Geotechnics carried out field investigations and have reviewed the submitted drawings, survey plan, photographs and engineered schematic designs of the as constructed retaining walls. The LRA therefore considers all aspects of the proposed use and development, including works that have been undertaken without obtaining relevant planning and building approvals.

Standard E6.5.2 Use likely to be exposed to a natural hazard

The proposed use does not meet acceptable solution E6.5.2 A1 (b) which requires residential use to be located on land where risk from exposure to a natural hazard is medium or less.

Performance criteria E6.5.2 P1 (a) ¹ requires a hazard risk assessment to demonstrate that a tolerable level of risk can be achieved and maintained for the nature and duration of the proposed use.

For the purposes of this analysis, risk to 'use' is considered to mean the same as risk to 'life' and is distinct from risk to 'development' or 'property'.

For the purposes of hazards pertaining to landslip, a hazard risk assessment is a landslide risk assessment which the planning scheme defines as an assessment and report prepared by a suitably qualified person, in accordance with the Australian Geomechanics Society - Practice Note Guidelines for Landslide Risk Management 2007 ('AGS Guidelines'). The LRA has been prepared in accordance with the AGS Guidelines.

Document Set ID: 1042381 Version: 1, Version Date: 12/04/2019

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¹ Performance criteria E6.5.2 P1 (b) is not applicable to the proposal because it is not for a critical, hazardous or vulnerable use.

The AGS Guidelines defines 'tolerable risk' as:

"a risk within a range that society can live with so as to secure certain net benefits. It is a range of risk regarded as non-negligible and needing to be kept under review and reduced further if possible"

The AGS Guidelines also provides criteria to quantify tolerable risk. The criteria is detailed in the table below.

Situation					Suggested Tolerable Loss of Life Risk for the person most at risk
Existing Developr	Slope nent (2)	(1)	/	Existing	10 ⁻⁴ / annum
New Constructed Slope (3) / New Development (4) / Existing Landslide					10 ⁻⁵ / annum

The LRA, at section 6.4, provides an analysis of the risk to life from landslide events in accordance with the tolerable risk criteria set out in the AGS Guidelines. The analysis included the preparation of probability event trees which are detailed in Appendix H of the LRA. The analysis concluded that provided the management measures recommended within the first event tree are complied with, the calculated risk to life is marginally lower than the tolerable loss of life for an existing slope.

As such, it is considered that performance criteria E6.5.2 P1 (a) can be met on the basis that the LRA has demonstrated that a tolerable level of risk can be achieved and maintained for the residential use subject to complying with the recommended management measures.

Standard E6.6.2 Development on land exposed to a natural hazard

The proposed development is only required to meet one of the acceptable solution provisions listed under clause E6.6.2 A1 (a) due to the presence of the disjunctive "or" after clause E6.6.2 A1 (a) (i).

The LRA, at section 6.3, concludes that the proposal meets the requirements of clause E6.6.2 A1 (a) (i) insofar as no specific hazard reduction or protection measures are required.

Acceptable solution E6.6.2 A1 (b) is not applicable to the proposal because it does not require land on another lot, outside of the site, for hazard management purposes.

Please do not hesitate to contact me should any further clarification be required.

Yours faithfully, 6ty° Pty Ltd

George Walker Planning Consultant



07/05/19

Rebecca Plapp Town Planner Waratah Wynyard Council PO Box 168 Wynyard Tasmania 7325

RE: Peer Review of Landslide Risk Assessment Report – 15 Hepples Road Boat Harbour

Rebecca, following review of the Landslide Risk Assessment Report prepared by Tasman Geotechnics dated the 9th of April 2019, I am able to report the following.

The report confirms that the site at 15 Hepples Road Boat Harbour is located on a mapped active landslide, and that the site is within a declared landslip A zone. The report represents a good snapshot of the geological conditions in the area, site observations, and a risk assessment to support the proposal.

There are a number of observations made in the report which are of particular cause for concern:

- "Houses adjacent to 15 Hepples Road (to each side and uphill) have been damaged by landslide movement as indicated by buckled walls, leaning columns, misaligning doors and windows".
- "A photograph of 15 Hepples Road before current reconstruction works also shows gaps in the external walls"
- "The ground surface of Hepples Road and concrete curbing has cracks and undulations indicative of ground surface movement"
- "Tension cracks were observed in the grass at 2 and 10 Hepples Road in 2016"
- At Hepples Road the landslide exhibits creep, approximately 45mm/year"

In relation to the recent works on the property there are a number of additional causes for concern noted in the report, with the following observation "we understand that bored piers were installed below the no-fines concrete retaining wall to 3m below the footing level. From our borehole profile, we expect this is at the top of the basalt bedrock. Therefore, the piers are not embedded in rock" followed by the interpretation of the geology "Talus is resting on steeply sloping bedrock consisting of basalt overlying quartzite. As groundwater is seeping out at beach level over the top of the basalt bedrock, particularly when groundwater is elevated, as is the case after high rainfall events". The two statements combined can lead to only one logical conclusion, that the retaining wall piers are not sufficiently embedded into bedrock to resist the sliding movement of the talus deposits promoted by groundwater flows. In relation to a second retaining wall on the property the report only states that "No construction details are available for the

other, a verti-block wall". As neither of the walls have been constructed with engineering designs or

certification, they cannot be relied upon to provide long term stability to the site, especially when the

Hepples Road landslide exhibits creep at approximately 45mm per year.

The above points in relation to the lack of engineering design and certification in the construction are of

particular importance to the risk assessment completed in the report which states "The risk assessment

shows that the risk to life for such those landslides and assuming management measures are incorporated

in the design and construction of the house is 9.7 x 10⁻⁵/annum". From the earlier conclusions in the

report that construction of the retaining walls is either unknown or have foundations not embedded into

rock would suggest that the design and construction does not have adequate management measures, and as

a result the risk assessment is fundamentally flawed. The actual risk to life and capital at the site is likely

to be in the tolerable to unacceptable range, and would require significant specialised investigation, design,

and certification to be acceptable.

Of what is most concern to the development is the content of Building Act 2000 and the building

regulations 2004 in relation to building works in a declared landslip A area. Building works including

erection of a house or alterations and additions to a building are prohibited on the property at 15 Hepples

Road Boat Harbour as it falls within a declared landslip A area. The risk assessment report concludes that:

"Thus, the works have carried out to date have contravened a number of limitations relating to an A

landslip area:

Adding or altering a house

• Carrying out building work

• Permanently excavating more that 600mm of soil"

The recent works on the site and the completion of any further works outlined in the development

application will be in clear contravention of the Building Act., and it is my understanding that a permit

authority must not grant development approval for works that would directly contravene another relevant

Act in the state of Tasmania. As a result, the only conclusion I can logically reach from review of the

report is that the proposed development on the site involves significant risk, is in direct contravention of

the Building Act, and should be refused.

Kind regards,

Dr John Paul Cumming PhD CPSS GAICD

Director

The General Manager

PO Box 168, Wynyard 7325

Waratah Wynyard Council

DA 53/2018

LOCATION 13 & 15 Hepples Road, Boat Harbour Beach

Land Use Planning and Approvals Act 1993

I Object to the Development Approval – Discretionary Matter

My objection/concerns are in green print

I believe that Suitability of the Site for the proposed development does not meet or cannot meet Acceptable Solutions v Performance Criteria for the following reasons;-

12.4.1(a) P1 Provide a suitable development area for the intended use

The land/property size is well below 500m square and the topography of the site further limits the available suitable land for a development site. Given consideration to normal setbacks from boundaries and the site being adjacent to the high water mark in normal circumstances and prone to yearly high and ebb tides, such set backs would make the proposed development too large and unsuitable for the site

The site is also located in a designated Landslip A area – refer to below documentation;-

Landslide Assessment for Boat Harbour Beach, Coffey Geosciences, March 2001. ☐ Land stability at Boat Harbour beach, WL Matthews (Mineral Resources Tasmania MRT report TR17_116_119) date January 1974. ☐ Preliminary report on landslides on the Boat Harbour Road by I B Jennings (MRT report designated TR9_107_108) date January 1965.

12.4.2

12.4.1 (b) Provide access from a road – the acceptable solution cannot be met because of the prevailing topography of the site both northern boundary (tidal beach) and southern boundary – a road in active landslip area. (As Above)

Re access road -

Considerable pre-approval works which included large amounts and volume of cut and fill, that have taken place from 2016 onwards have affected the site with considerable land movement and specifically affected the main access road (Hepples Road) in the immediate area that adjoins the sites, specifically the site 15 Hepples Road

**A site visit can immediately confirm this comment. The road has an engineering marker that is currently under observation by the Council's Engineering Department.

This site cannot be deemed a suitable development area for the intended use?

The northern boundary of the property is beachfront and subject to tides that prevent any access to the site, except at absolute low tide and the beach not able to provide access for large trucks for building materials, concrete, windows etc.

12.4.2 Dwelling density

Make efficient use of land for housing –

- (a) suitable building area no as above
- 12.4.2 (b) Utilities and community services no water supply, no storm water provisions, no sewerage given scale of proposed building v site size

Where can provision for water supply occur without any setbacks from boundaries adhered to.

12.4.3 -

(b) Adjacent home on Western boundary already with approx 1 m from current building. Given the High tide mark, on boundary as per the applicants drawings — house setback from Hightide mark, neighbouring building (western

Boundary) not sufficient land size to allow development, setbacks cannot be observed with the size and scale of the proposed development.

E4.6.1

Change in exisiting ground level – Landslip A – no criteria met

I object

**Cut and fill and considerable excavation for footings have already taken place and considerable and current land movement still being observed. (As previously commented under 12.4.1

Does/would Retrospective approval cover the following;-

W. M. andrusto

Have geotechnical engineers/surveryors approved the works that have already taken place and observed any technical and detailed plans and drawings of said work, is it/can it be confirmed these works have meet all possible engineering and building criteria and are they satisfied the work has work performed to acceptable standards as to not further acerbate the nature/topography of the site and most specifically that of the adjoining road, Hepples Road.

Is Council satisfied that all criteria has been met and can guarantee that works that have taken place and works that are listed in the Application will not further acerbate the vialibity of Hepples Road.

Signed,

Wendy M Andrusko

8 Hepples Road,

Boat Harbour Beach

Agreement for Extension of Time

In accordance with Section 57 (6) of the Land Use Planning and Approvals Act 1993 I

6ty Pty Ltd

of

PO Box 63 RIVERSIDE TAS 7250

hereby grant the Planning Authority an extension of time until the 24th day of May 2019, Ref. No. 7087735 & DA 53/2018

Signed

GEORGE WM WER (Applicant)

9 - 4 - 2019 (Date)

Signed

DANIEL SUMMERS, per Council delegation

(Director of Infrastructure & Development Services)

14.03.2019 (Date)